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SILICON SOLAR CELL PROCESS
DEVELOPMENT, FABRICATION AND ANALYSIS

Final Report

CDRL #6

JPL Contract No. 955055

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The JPL Low-Cost Silicon Solar Array Project is sponsored by the U.S. Department of Energy and forms part of the Solar Photovoltaic Conversion Program to initiate a major effort toward the development of low-cost solar arrays. This work was performed for the Jet Propulsion Laboratory, California Institute of Technology by agreement between NASA and DOE.

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#### ABSTRACT

Solar cells have been fabricated from unconventional silicon materials in the second and final phase of the contract.

In the most recent period of week, EFG, Web, Hem, and Continuous CZ silicon materials were fabricated into solar cells, measured and analyzed.

Current-voltage measurements under AM1 conditions, in addition to those under AM0 conditions, were introduced in Phase II.

Several low-cost fabrication steps were included in that phase.

Both Hem and Continuous CZ silicon were found to be superior to what had been provided in Phase I. Correlation between quality of starting materials and cell conversion efficiency was observed for Hem-grown silicon. Correlation between position in the crystal growth sequence and cell quality was observed for Continuous CZ.

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#### 1.0 INTRODUCTION

The goal of this contract has been to conduct a silicon solar cell process development, fabrication and analysis program. The effort being directed toward the evaluation of the solar cell potential of unconventional silicon sheets of interest to the Large Area Silicon Sheet Task of the Low-Cost Solar Array Project. What has been required has been the fabrication of a statistically significant number of solar cells using standard and reproducible processes and reliable testing of them using standardized measurement equipment and techniques. In addition, to investigate, develop and utilize technologies appropriate and necessary for improving the efficiency of solar cells made from these silicon sheets using a standard process as the baseline starting point. The goal for solar efficiency is 12% Air Mass Zero (AMO), measured at 28°C minimum.

In this report we shall provide a review of the control program, baseline processing, various optimization processes, the measurement systems/procedures and a brief description of the unconventional silicon materials in the program. We shall then report on results obtained since the last published report. This will then be followed by a brief review of results in Phase I and Phase II of the contract.

#### 2.0 TECHNICAL DISCUSSION

A number of diverse silicon materials have been made into solar cells by both conventional and optimized processing methods during the period of this contract. In order to provide a reasonable amount of reproducibility within each material group of cells, a specific control program was mandated. It was believed that this control program would minimize the occurrence of wafer contamination from extrinsic sources. Because elevated temperatures are used and since contamination is sustained via a thermal pathway, emphasis was given to reduction of contamination before and during the impurity diffusion process.

#### 2.1 CONTROL PROGRAM

Quartz diffusion tubes dedicated to the program were used throughout the study. After cleaning a diffusion tube the tubes were then used in processing control wafers into solar cells. The finished solar cells were measured for I-V on a solar simulator and if the results were satisfactory the tube was then considered contamination-free and used for thermal diffusion of one of the unconventional materials into solar cells. In the event the control cells were found not to be satisfactory, the diffusion tube was again cleaned and the process repeated until suitable control cells were obtained. At no time were different sheet materials run together in the same diffusion tube, and only after the above control procedure had been satisfactorily completed would a tube be used for a different sheet material.

During processing of the sheet materials control cells were included. Within the diffusion tube eight control wafers were

positioned on the quartz diffusion tube such that every unconventional silicon wafer had a control wafer neighbor. Control wafers were also positioned at the front and back of the wafer assembly on the diffusion boat.

These same control wafers accompanied the lot throughout fabrication and measurement. Such a procedure also allowed a means of comparison and some indication of processing fidelity.

#### 2.2 PROCESSING FORMAT

The unconventional silicon material was supplied by the Jet Propulsion Laboratory. CZ, p-type,  $\sim 2\Omega$  cm silicon control wafers were produced in Spectrolab's crystal growing and cutting facilities. After cutting of the material into slices both the front and back of the slices were etched sufficiently to remove saw damage. This was not required for the material that had been grown in sheet form. In the latter case various cleaning methods, including acid etch, were used to remove surface stains that might have been present. The slices, or ribbons, were then diced to their planar wafer dimensions on a Tempress saw.

After cleaning to remove both organic and metallic surface impurities, the wafers were loaded onto a clean quartz boat and placed within a three-inch diameter quartz diffusion tube maintained at the diffusion temperature (850°C) by a Thermco furnace. The diffusion schedule was arranged such that the wafers were loaded and in the furnace within an hour of the wafer cleaning.

A three step diffusion procedure was used: warmup (nitrogen flow), pre-dep (phosphine, nitrogen, oxygen flow), and drive (oxygen and nitrogen flow). These conditions were expected to result in a

phosphorous surface concentration in excess of  $10^{20}$  cm<sup>-3</sup> and pn junction depth of  $\sim .35 \mu m$ . Following the diffusion drive the boat was removed from the furnace and allowed to cool in air.

After diffusion and cool the wafers were immersed in an HF solution to remove the thermal oxide. Sheet rho was then measured on a four point probe to obtain an estimate of junction depth. The fronts of the wafers were then masked and the wafers passed through an acid shower. This was used in order to remove the n-diffused region on the back surface of the wafers. After removal of the etch mask the wafers were cleaned in various solutions, loaded in an evaporation mask and holder and placed in the chamber of a high vacuum system. Using an electron-beam heating source, thin layers of titanium, palladium and silver were deposited on the wafers in a contact pattern defined by the masks. After removal from the evaporation system and masks, the wafers were sintered in a hydrogen atmosphere to minimize contact resistance. The cells were then placed in an electron-beam evaporator where an AR film of Ta<sub>2</sub>O<sub>5</sub> was deposited.

In the next and final procedure the wafers were masked with an organic film over top and bottom surfaces. In this state the cells were immersed in a solution to remove any metal or other undesirable contaminant that could cause low shunt resistance at the cell edges. The cells were cleaned and made ready for measurement.

#### 2.3 MEASUREMENT SYSTEMS

# 2.3.1 Illuminated Current-Voltage

This system is shown schematically in Figure 1. The Spectrosun Solar Simulator is adjusted to produce an AMO spectrum and intensity. Temperature and intensity calibration for each group of

I-V measurements is made by adjusting water bath temperature and simulator intensity while monitoring these parameters with the #1037 balloon-flown solar cell standard.

The cel. test fixture is water cooled, uses a vacuum hold-down and has spring-loaded voltage probes and spring-loaded current probes for cell top contact. The fixture itself makes electrical contact with the bottom of the cell. A Spectrolab Model D-550 electronic load is used in series with the cell under test. Both short circuit current and open circuit voltage are measured by means of a 4½ digit Dana Digital Voltmeter. The I-V curve is generated by the electronic load and recorded on a Hewlett-Packard X-Y Recorder.

AMI measurements are obtained by introduction of a constant temperature Pyrex-water filter into the light path between the Xenon source and the water-cooled test fixture. After insertion of the filter into the system the light source is adjusted using a standard solar cell, #1039, that has been calibrated to Air Mass One. The filter is tilted slightly from the horizontal to prevent reflection of the radiation back into the source.

## 2.3.2 Spectral Response

This system consists essentially of a water-cooled test fixture enclosed within a light box. A broad spectrum, high intensity light source impinges upon a filter contained within a filter wheel. Narrow-band radiation is transmitted through the filter and onto the tor surface of the cell under test. The short circuit current is measured by amplifying the voltage across a low value precision resistor and reading the amplified voltage on a Dana 5 digit Digital Voltmeter.

The filter wheel consists of thirteen narrow band-pass filters incremented across the spectrum from .4 to 1.05  $\mu m$ .

Irradiance at the cell surface for each of the thirteen filter positions is measured using a calibrated solar cell. Based upon the irradiance and output of cell under test the relative response can be determined for the cell under test at each of the thirteen wavelengths.

## 2.3.3 Dark Current-Voltage

Dark current, forward and reverse, is measured on a system consisting of a high resolution constant current supply, a light shielded brass test fixture, and two 5-digit Dana Digital Voltmeters. Measurements are made point-by-point using voltage as the independent variable.

### 2.3 Resistivity

Wafer resistivities are measured by means of a four point, inline probe and micrometer thickness gauge. The in-line probe is also used to measure sheet resistance after diffusion.

### 2.4 UNCONVENTIONAL SILICON MATERIALS

## 2.4.1 Wacker Silso

Wacker Silso polycrystalline silicon is a product of the Wacker Siltronic Corporation. It is produced by casting molten silicon into rectangular blocks. Casting is controlled so as to promote columnar grain growth such that grains grow perpendicular to the plane of the finished cut sheet. The casting is sawed into sheets of square form. This material was used for solar cell fabrication in Phase I of the contract.

# 2.4.2 Ribbon-to-Ribbon (RTR) Silicon

This material is a product of Motorola and is produced by a process that deposits silicon upon strips of substrate material by CVD. The resultant silicon strips are then laser or electron beam scanned to promote grain growth from the extremely small grains obtained during CVD deposition. A phosphorous gettering step completes the process. The strips used in this contract were about an inch in width and 12 inches in length. This material was used in Phase I of the contract.

# 2.4.3 Edge-Defined Film Fed Growth (EFG) Silicon

This polycrystalline silicon is produced by Mobil-Tyco. Silicon strips are pulled through dies (SiC) from the melt with widths in excess of two inches and lengths greater than four inches. The finished sheet has a smooth, somewhat rippled surface. Both rf heated and resistance heated systems have been used in the production of the sheet material, only resistance heated material was used in Phase II of the contract.

# 2.4.4 Dendritic Silicon Sheet (Web)

Web silicon is produced for the program by Westinghouse Research and Development Center. This sheet material is manufactured by supporting a silicon meniscus between two dendrite rails which are slowly lifted out of the melt. The silicon solidifies as it is lifted and this forms a continuous sheet of material. The surface of the drawn filament, or ribbon, is in the 111 plane. Thickness of the filament is well controlled and width is determined by the spacing of the dendrite rails. Web material used in the program was generally in widths of about one inch while thicknesses ranged from 4 mils up to 12 mils.

# 2.4.5 Heat Exchange Method (Hem) Silicon

This material is produced by Crystal Systems, Inc. In this method a seed crystal is placed at the bottom of an insulated chamber. An inert gas is used as a heat exchanger for the seed and precludes its loss when molten silicon is injected into the chamber.

The freeze boundary of the cooling silicon proceeds out from the seed, generally with growth of a single crystal. Directional solidification, proceeding at a very low rate (depending upon how well heat exchange is controlled), will cause those materials having low segregation coefficients to segregate and thus be moved along with the freeze boundary toward the outer surfaces of the boule. The boule is generally formed in a rectangular shape. Rectangular slices are then cut from the boule.

# 2.4.6 Continuous CZ Ingots

This material is produced by the Kayex Corporation. In the conventional CZ method a single crystal is pulled from the melt contained in a quartz crucible. The pull of one crystal completes the operation and the crucible is treated as an expendable at a rate of one crucible per pulled crystal. In the continuous CZ method several crystals are pulled in sequence from a single crucible. The melt in the crucible is replenished after each pull. In Phase I of this contract, material from a five crystal pull run was processed into cells while in Phase II material from a nine crystal pull was processed into solar cells.

## 2.4.7 Silicon on Ceramic (SOC)

This method of producing unconventional silicon has been developed at the Honeywell Corporate Research Center. Slotted

ceramic substrates coated on one side are either dipped into or skimmed over molten silicon, leaving a coating of polycrystalline silicon on the ceramic. Although this material was received under Phase I and Phase II, cell fabrication and measurement were not completed within the time and funding limits for the contract.

#### 2.5 PROCESS OPTIMIZATION

Process optimization in this program is proposed in the sense of both general and specific methods that might be expected to enhance device performance over and above what was achieved by the baseline process. Optimization procedures were limited, however, by the large number of materials studied and the size of the program. With this in mind a number of optimization steps were used for each of the silicon materials in the program.

# 2.5.1 Texturization

This process modification has two functions. The primary one is the reduction of surface reflections while the second is to increase absorption in the immediate region of the junction.

Surface texturization is the result of directionally selective etching of a wafer surface that leaves a matrix of pyramids at the surface. (In Figure 2 we show a photograph of a typical texturized surface.) This matrix promotes transmission of reflected primary rays. Solar cell surfaces that have been both texturized and coated with an antireflecting film appear mattelike to the observer. Since the index of refraction of silicon is high, and since the pyramids present a surface of about 45° to the normal incidence, normal rays are refracted away from the normal to the wafer plane. The result of this

refracted path for the transmitted radiation is a longer path of light with wafer depth and hence enhanced absorption near the junction.

Texturization is most effective for (100) silicon and ineffective for (111) silicon. Since dendritic web silicon is grown with a (111) surface this optimization procedure was not used on that material. For the polycrystalline material the effectiveness of texturization varied according to the orientation of individual grains.

# 2.5.2 Back Surface Field

In this procedure a P region is processed onto the back side of the wafer. This P region serves a number of purposes. It creates an electrostatic reflector in the lower base region and reduces contact resistance. The electrostatic reflecting properties should increase short circuit current and reduce dark currents that arise by recombination at the back surface. This should, in turn, increase open circuit voltages. In addition to the obvious requirement that the electric field generated by the P P configuration be of a sufficient magnitude the distance from the junction to the P P boundary region, vis a vis the minority carrier diffusion length, must be within certain limits. For a given  $\chi_{\tau}$  to P P distance, a threshold minority carrier diffusion length exists to observe the effect. Therefore, materials with short minority carrier diffusion lengths cannot be expected to be enhanced by a back surface field. One could, of course, speak of a threshold  $\chi_{\tau}$  to P P distance for a given L<sub>D</sub>.

# 2.5.3 Junction Depth

Historically, junctions of space solar cells have followed a course of decreasing depths. An observer could speculate that

this has been the result of a somewhat gradual realization that photons absorbed above the junction are wasted. Shallower junctions have required heavier doping in the top layer and improved contact systems because of the increased sheet resistance that accompanies the shallow junction. Improved diffusion methods have also accompanied the shallower junctions providing a somewhat higher minority carrier lifetime in the top layer. Recently, efforts at reducing surface recombination velocities on silicon solar cells have shown some degree of success.

Shallow junctions are of greater efficacy at AMO because of the relative portion of that spectrum in the blue and violet. Though it is less of a factor for cells to be employed at terrestrial sites, it is still possible to enhance collection efficiency of terrestrial cells by means of shallow junctions. Shallow junctions, however, increase the risk of junction leakage and result in lower production yields. With these caveats in mind shallow junctions were utilized in several optimized processing runs.

### 2.5.4 Gettering

It is well known that certain types of "gettering" can enhance performance of silicon devices. Gettering is believed to result because of an out-diffusion and trapping of various secondary impurities at gettering sites. The type of secondary impurities that combine with lattice structure defects to produce recombination centers are in most cases fast diffusers and are trapped at regions of structural damage and strain. Various experimental work has shown that phosphorous precipitates generate high strain, dislocation tangles, etc. This highly damaged region in the top layer of the silicon device leads to very short minority carrier

lifetimes in volume immediate to the surface. At the same time, however, it tends to clean up the rest of the device, especially the junction region.

Evidence for the effect of secondary impurities on device performance has been shown by, amongst others, experiments of Goetzberger and Shockley (2). Specific evidence for mechanisms in the junction region have been described in the SEM-EBIC experiments of Varker and Ravi (3). Murarka (4) has identified the phosphorous gettering action on trace impurities of gold using neutron activation analysis. The latter work shows conclusive evidence that the gettered specie (gold) is trapped within the surface region of the precipitates and not within the phosphorous glass.

### 2.6 PHASE II

A number of changes were made in the program going from Phase I to Phase II. The first of these changes was I-V measurement at AM1 as well as at AM0, for about 20% of the cells. This was done to provide measurements more meaningful for terrestrial application, and to provide empirical relationships between AM0 and AM1 efficiencies for the cells fabricated in the program. A second change was the use of processes that could be considered low cost, as opposed to the methods of Phase I that were based upon aerospace manufacturing processes. A third change was a somewhat more general use of the cell areas greater than 2 cm x 2 cm. Finally, a record was made of the steps in the processing where cell breakage occurred. This was suggested as a means of determining any critical breakage points in the processing for a specific material.

### 2.7 RESULTS

# 2.7.1 Westinghouse Web

In this section we report results for three lots of solar cells fabricated on dendritic web-grown silicon utilizing processes intended to enhance conversion efficiency. In the first of these lots, Web0-1, cells were 2 cm x 4 cm and had back surface field processing. Results obtained from illuminated I-V at AMO and AMI are presented in Table 1.

In a second lot, Web0-2, also with BSF, cells were made in a 2 cm x 2 cm configuration. Results obtained for illuminated I-V measured at AMO and AMI are shown in Table 3. It is apparent that the latter BSF were more effective in improving cell efficiency than in the case of lot Web0-1. This can be attributed to insufficient heating of the substrate during the high temperature anneal following deposition of aluminum paste for the BSF. The warmup of the wafers is dependent upon furnace temperature, boat configuration and wafer size. To produce the back surface field the wafer temperature must surpass the Al-Si eutectic temperature over the whole of the wafer area. In Figure 3 we show those cells with BSF having the highest efficiency of the cells in each dendritic web strip. Other noteworthy differences between the two lots can be seen in the open circuit voltages. In Web0-1 we find  $\rm V_{\rm OC}$  of the order of 530 mV and 545 mV for 9 N-cm and 3 N-cm cells as compared with 555 to 585 for the 13 Nacm web materials in lot Web0-2. Another factor of importance in comparing these two lots is the difference in wafer thicknesses. The lesser thickness in Web0-2 cells would be expected to enhance the effect of the back surface field. Diffusion length would of course be expected to play a noticeable role in the effects promoted by wafer thickness.

A third and final web optimization lot, Web0-3, was made using a shallow junction. Measurements for the completed cells are given in Table 5. Cell size used in this lot was 2 cm x 4 cm. Spectral response data has been plotted for a number of cells in Figures 4 and 5. Blue response is equivalent for the Web and CZ cells, but a rather extensive divergence for red response is seen between the two materials. This suggests considerable differences in minority carrier diffusion lengths between the two materials.

We examine this difference by calculation of the effective diffusion lengths from spectral response measurements  $^{(5)}$ .

| S/N   | LD     | Υ     |  |
|-------|--------|-------|--|
| X-1   | 223 um | .9997 |  |
| X-5   | 209    | .9995 |  |
| 191-1 | 79     | .9993 |  |
| 187-1 | 71     | .9995 |  |
| 171-1 | 79     | .9995 |  |
| 171-3 | 74     | .9994 |  |

## 2.7.2 Mobil-Tyco EFG

Lot EFG0-2 was intended as an optimization of cell characteristics by means of a back surface field. Application of the back surface field structure to the cells was by screen printing of aluminum paste followed by a high temperature anneal for a brief period (spike anneal). Processing of the cells in this lot met with a continuous series of misfortune. Breakage for the cells in the lot was widespread. Six of ten control cells and three of about thirty-five EFG cells were unbroken. As can be seen in the tables for this lot (Tables 7 and 8) breakage occurred

at most steps of the cell processing. Although breakage has not been found unusual for the EFG material, results in this lot indicate a high degree of fragility. Breakage losses were also unusually high for the control cells, however. In comparing losses in this present lot with those of previous lots, one must conclude that faulty processing must account for a large share of the breakage. Cell data for the lot is given in the tables. Illuminated I-V characteristics are lower than expected for both the EFG cells and control cells.

## 2.7.3 Crystal Systems Hem

Silicon wafers by the heat exchange method have been fabricated into solar cells by methods intended to improve the solar conversion efficiency over the cells fabricated by the baseline method. Some of these methods are considered to be low cost. A base etch was used in place of the usual conventional acid etch for removal of saw damage and control of wafer thickness. A back surface field has been applied to the cells for increased  $V_{\rm oc}$  and  $I_{\rm sc}$ .

Lot Hem0-2 was fabricated to determine the effectiveness of the back surface field on this material from a specific Hem crystal (342C) and also to see what, if any, enhancement could be expected by using a thinner wafer thickness. The lot consisted of 9 mil cells made using back surface field cells, 9 mil cells made by the baseline method, and 5 mil cells made using back surface fields.

Results for the lot are given in Tables 9 and 10.

Comparison of I  $_{\rm SC}$  between baseline and back surface field processing indicates a definite enhancement for the latter cells. In the case of the control cells  $\rm V_{\rm OC}$  enhancement is also observed although this is not the case for the Hem cells. Lack of  $\rm V_{\rm OC}$ 

enhancement for the Hem cells is not too surprising, however, since resistivity was determined to be less than 1  $\Omega$ -cm.

In Figure 6 we display data for average values of the spectral response from 6  $\mu m$  to 1.05  $\mu m$  for the 5 mil-BSF, 9 mil-BSF and 9 mil-baseline. One observes the current enhancement of the cells having back surface fields. In Figure 7, percent enhancement of 9 mil BSF cells over 9 mil baseline cells is shown (average values). As one would expect, enhancement is greatly increased for current generated by photons absorbed deeper in the base region of the cell (and hence the path described by distance from absorption site to BSF + distance from BSF to junction is less for longer  $\lambda$  photons, on average).

L measured from spectral response on the following baseline cells in Hem0-2 is given  $below^{(5)}$ ,

| S/N | L   | Υ     |  |  |
|-----|-----|-------|--|--|
| C-7 | 200 | .9987 |  |  |
| 14  | 100 | .9998 |  |  |
| 15  | 80  | .9992 |  |  |
| 12  | 70  | .9995 |  |  |

Diffusion length calculations suggest variation in Hem material within crystal sections. (Exact location of section in crystal 342C was not noted by processing personnel.)

Two lots of cells were fabricated from the Hem silicon to determine the effect of impurity gettering on this material and what this might do insofar as efficiency optimization is concerned.

In the first of these lots, Hem0-3, the wafers were phosphorous diffused in the usual manner. The wafers were then etched

sufficiently to remove the diffused n layer. The pre-diffusion clean was repeated and the wafers were again diffused. Processing was continued by the baseline method and the fit shed cells were measured.

In the second lot, Hem0-4, the processing used in Hem0-3 was duplicated with the exception that the diffusion drive time in the first diffusion was extended by a factor of three.

Results for both of these lots are given in Tables 11, 12, 13 & 14.

In Figures 8, 9 and 10 we show a histogram of the crystals for the various I-V parameters in the three lots. One may draw several conclusions from these figures. The first of these is that cells made from silicon material in crystal 349 had degraded properties in the runs with the extra gettering step. The results for cells from material in crystal 342 indicate little or no change. Results for cells from material in crystal 314 indicate a definite improvement, especially evident in the Hem0-4 results.

A disturbing feature of these results is the high  $\rm V_{oc}$  for this material (1.4  $\rm G-cm$ ). One would expect a maximum of 590 for such resistivity.

As a specific group, cells made from crystal 349 without an added diffusion step (gettering) had the best conversion efficiencies.

Crystals 349 and 342, with resistivities in the range of .4 to .8  $\Omega$ -cm, were grown from high purity melt stock. Crystal 314, with resistivity of 1.4  $\Omega$ -cm, was grown from float zone remelt stock. One can account for the higher open circuit voltages of the former by the lower resistivities. The reduced short circuit

currents and efficiencies obtained for solar cells fabricatelon crystal 314 material could result from the increased secondary impurities one would expect to be contained in float zone remelt stock.

## 2.7.4 Kayex - Continuous CZ

Material for solar cell fabrication in Phase II of the contract came from run 62 of the Kayex effort. Nine crystals were pulled from a single crucible in run 62. The crystals were of the order of five to six inches in diameter and were sliced to give representative portions of the top, middle, and bottom sections of each crystal.

Two baseline runs were made on this material. Since this was CZ material the primary interest here was to determine how the cells from this material compared with conventional CZ grown material, how cells fabricated from top, middle and bottom sections of a crystal compared and finally how cells from one crystal compared with cells from other crystals in the pull sequence.

Illuminated I-V results for the first baseline run, HamcB-1, are given in Table 15. A and B prefixes denote cells from slice A and slice B. Both slices are from the top section of crystal #1 in Kayex run 62. Dark current data are given in Table 16 and spectral response data are given in Table 17. Comparing the Kayex CZ with the control CZ cells one observes a higher solar conversion efficiency for the latter. In Figure 11 a comparison of spectral response is made between the cells with highest efficiency in slice A, slice B and the CZ control cells. This group of curves implies a slightly greater minority carrier diffusion length for the control CZ silicon.

In the second baseline run, HamcB-2, cells were fabricated from slices cut from five different crystals in Kayex run Number 62. Data for illuminated I-V, spectral response and dark current are presented in Tables 18, 19, and 20, respectively. A modification in this run was the use of NaOH (30%) etchant in place of the usual acid etch to remove saw damage and thin the wafers to 9 mils, but without surface texturizing.

In Figure 12 the distribution for conversion efficiency is plotted for the Kayex CZ cells and for the control cells. The distribution for both groups is similar. The Kayex cells are identified as to the location they occupied in the crystals; top, middle, or bottom. Distributions for efficiency are plotted for the cells and separated by crystal source. Control cell efficiencies are clustered about 11.5% whereas the Kayex CZ cells are clustered about 11%. Cells from bottom sections of crystals 7 and 9 represent the lowest efficiencies for the Kayex group. Three of the four low efficiency cells are polycrystalline while the cell with the lowest efficiency had arrays of deep etch pits across its surface.

In Figure 13 spectral response data for a number of the cells has been plotted. Cells fabricated from top sections of the crystals group about the control cell C-1. The bottom of crystal number 1, middle of crystal nine, bottom of crystal number 7 and bottom of crystal number 9 have reduced spectral response, with the bottom of number 9 occupying the position of lowest response.

Such an order is not unexpected since the secondary impurities would be segregated out of the growing crystal and into the liquid silicon remaining in the crucible. The density of impurities remaining in the crucible would increase with growth causing the concentration of impurities to be higher at the bottom end

of the crystal. With the addition of more silicon before the next crystal pull, the impurities would be diluted hence the top of the next crystal should be "cleaner" than the bottom of the previous crystal. Going from the first crystal to the ninth crystal one would expect a gradual increase in impurities in the melt. An increase in the concentration of secondary impurities in the crystal would reduce the minority carrier diffusion length and this would be apparent in a reduced long wavelength spectral response. In Figure 14 the percent reduction in spectral response for the various crystal sections is shown, at .8 mm and at .9 mm, where the average response for cells from top sections of the crystals serves as the benchmark value.

Although there is evidence of reduced diffusion length as growth proceeds from beginning to end, the effect on conversion efficiency is apparent, yet not large.

In the next fabrication lot the cells were made incorporating a back surface field. Illuminated I-V data for this run, HamcO-I, are given in Table 21. Spectral response and dark current data are given in Tables 22 and 23, respectively. In Figure 15 open circuit voltage and short circuit current are plotted for the cells in this run. Baseline values, derived from runs HamcB-1 and HamcB-2, are given for comparison. There is a general enhancement in both open circuit voltage and short circuit current for both the top and middle s ction cells with the greater enhancement for the former. For the bottom cells there is some short circuit current enhancement but none for open circuit voltage. Cells below the baseline had shunting and/or series resistance indications in their illuminated I-V curves.

In Figure 16 conversion efficiency at AMO is plotted for run HamcO-1. The enhancement by the BSF is in evidence here with

greatest percentage enhancement for cells from top sections and least enhancement for cells from bottom sections. In the final figure for this section, Figure 17, spectral response is presented for several cells having the best efficiency in their respective group. From this plot one observes the degree of enhancement provided by the back surface field for a given cell thickness and minority carrier diffusion length. The greater enhancement can be easily seen for the longer diffusion length material.

### 2.8 AIR MASS ONE I-V CHARACTERISTICS

As stated in Section 2.6, I-V measurements at AM1 were instituted in Phase II of the contract for 20% of the cells. This was done to obtain more relevance for terrestrial application and to determine an empirical relation between AM0 and AM1 characteristics for cells of this type. AM1 measurements were made on the Spectrolab solar simulator (X-25) with a Pyrex water filter in the optical path and calibrated against a standard cell, #1039, traceable to NASA standards. Results are presented below for  $^\eta AM0/^\eta AM1$ . On several occasions the efficiency ratio was found to diverge sharply from  $^{\circ}1.17$ . Generally, this could be traced to measurement or calculation error.

Results for efficiency ratio measurements are given below.

|            | N   | R    |
|------------|-----|------|
| Hem        | 29  | 1.17 |
| Web        | 36  | 1.18 |
| Kayex      | 24  | 1.18 |
| Control CZ | 41  | 1.17 |
| Composite  | 130 | 1.17 |

where N = number of cells

 $\overline{R}$  = average value of R

 $R = \eta_{AM1}/\eta_{AM0}$ 

## 2.9 CONCLUSIONS

Cells fabricated from Web silicon were somewhat broad in their distribution of efficiencies. This would be expected since the web material was itself rather varied in both resistivity and minority carrier lifetime. The back surface field was found to be effective in enhancing the open circuit voltage, as in lot Web0-2 where 12  $\Omega$ -cm web material had open circuit voltages of 580 mv. Spectral response measurements have shown the wide differences in diffusion length between the CZ control material and some of the web material used in these few lots as they have also shown differences in the diffusion length from one web strip to the other.

For the Hem material we have found a variation in cells fabricated from different crystals. The crystals we have used represent but a small fraction of the boule so what we have found must be qualified by that condition. As would be expected the "cleaner" the starting material the higher the cell efficiency. Some of the Hem material was apparently equivalent to the CZ material used for control cells. The low resistivity material, in some instances, when fabricated into cells had open circuit voltages greater than 600 mv and with BSF some enhancement in current was observed. Gettering did not appear to offer enhancement of the cell efficiencies.

The continuous CZ material was found to produce reasonably good cells with some fall-off in efficiency from the top to the bottom of the crystals. The fall-off in diffusion length from the first to the last crystal was obvious from the spectral response curves, however its effect upon conversion efficiencies was not so apparent. Only when back surface fields were applied was the reduced diffusion length significant as a factor that attenuated the effect of the back surface field.

#### 3.0 REVIEW OF PHASE II

Phase II has followed a path very similar to Phase I. In essence much of the work was a repeat with some variations. Most of the size etching was done using NaOH etchant in place of the usual acid etchant. This was a part of the low cost thrust. It had limited significance on the outcome of the various lots.

Screen printed contacts were tried on cells fabricated from EFG material but the effect was to degrade the cell performance. It became obvious that screen printed contacts could be a program in its own right since several of the materials could not be printed without some very specific fixtures and problems.

The most significant outcome in this phase would have to be associated with the Hem material and the continuous CZ silicon. In the case of the former, some Hem crystals were found to provide cells with performance on a par with CZ control cells and showed a dependence upon the quality of silicon material being processed by the heat exchange method. It did not, and could not, show uniformity or the lack of uniformity in the Hem boule because only small sections of each crystal were provided.

In the case of the continuous CZ material, considerable improvement was evident in the Phase II material over the Phase I material. In Phase I, with fewer and smaller crystals pulled, only top sections were single crystalline and only those produced quality cells. The Phase II product, however, consisted of more and larger crystals in a single run, and most parts of the crystals had the potential for quality solar cells. Only in bottom sections was optimization limited.

The EFG material was not better than the resistance heated source material in Phase I. It would have been more productive to have had some of the material developed with controlled  ${\rm CO}_{\bf x}$  atmospheres and reported on by Mobil-Tyco.

### 4.0 SUMMARY AND CONCLUSIONS

In this section we provide a table containing maximum conversion efficiencies for each material throughout Phase I and Phase II of the program. Data are displayed graphically in Figure 18.

We note from this table that of the expressed Phase I contract goal of 12% AMO at 28°C, three of the materials reached or surpassed the goal, namely: dendritic web, Hem, and continuous CZ.

LIST OF CELLS HAVING HIGHEST EFFICIENCY FOR THEIR MATERIAL GROUP

|                      | n %<br>(AMO)    | Jsc                 | Voc        |              |         |                     |            |
|----------------------|-----------------|---------------------|------------|--------------|---------|---------------------|------------|
| Material             | (28°C)          | ma cm <sup>-2</sup> | (mV)       | FF           | Lot     | S/N                 | Comment    |
| RTR<br>Control*      | 7.2<br>11.6     | 23.6<br>36.3        | 559<br>588 | .74<br>.73   | RTR-2   | 5<br>C-7            | Baseline   |
| EFG-RF<br>Control*   | 9.8<br>8.9      | 31.3<br>35.5        | 567<br>563 | .75<br>.60   | EFG-3   | 46<br>C-5           | Baseline   |
| EFG-RH<br>Control*   | 8.4<br>11.9     | 29.0<br>35.8        | 537<br>586 | .73<br>.77   | EFGB-1  | D<br>6              | Baseline   |
| Wacker               | 10.6            | 33.5                | 554        | .77          | W-4     | 4                   | Baseline   |
| Silso<br>Control*    | 12.5            | 35.5                | 598        | .79          |         | 2                   |            |
| Web<br>Control*      | 12.0            | 37.3<br>37.0        | 579<br>596 | .75<br>.80   | Web-5   | 6<br>Н              | BSF<br>BSF |
| Hem<br>Control*      | 12.3            | 34.8<br>35.8        | 605<br>589 | .790<br>.778 | HemB-1  | 349<br>S2 E1<br>C-3 | Baseline   |
| Cont. CZ<br>Control* | 12.6<br>All Shu | 36.8<br>nted        | 602        | .770         | Hamc0-1 | 9T2                 | BSF        |

<sup>\*</sup>Control cell with highest n in the same lot.

The RTR and EFG materials used in this contract are now obsolete. Claims by both sources of these materials indicate that considerable improvement in quality has been attained. The Wacker material

could probably be brought to higher efficiencies than reported here by using thirner cells in conjunction with back surface fields. There was a noticeable drop-off in efficiency at the corners of the Wacker sheet due to either reduced grain size or oblique grain boundaries.

The web material would appear to have considerable potential for high quality cells. The ability to control the sheet thickness as well as resistivity and lifetime would rake this material a formidable contender in the high efficiency cell class.

The heat exchange method has shown itself to be capable of producing quality solar cells. This is especially true when clean polysilicon is used as the starting material. How uniform the quality is throughout the grown crystal has not been shown. The method also appears appropriate for growth of solar material from starting material that could only be classed below semiconductor grade polysilicon.

The continuous CZ method employed to produce some of the material in the contract does appear to have considerable potential. The consistent results from top to bottom and crystal to crystal and the overall improvement from Phase I material to Phase II material supports this outlook.

#### 5.0 ACKNOWLEDGEMENTS

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## 7.0 TABLES

## Table 1

|                |   |  |                    |         | INATED CHAR        |                |                |                |          |   |
|----------------|---|--|--------------------|---------|--------------------|----------------|----------------|----------------|----------|---|
|                | 1000                                    |  |                    |         | EB01               |                |                |                |          |   |
|                |   |  |                    |         |                    |                |                |                |          |   |
| *              |   |  |                    |         |                    |                |                |                |          |   |
|                |   |  |                    |         |                    |                |                |                | 7        |   |
|                | CELL                                    | _NAME                                  |                    |         |                    |                |                |                |          |   |
|                |   |  |                    |         |                    |                |                |                | 6.000    |   |
|                |   | (CM2)                                  | 4.000              | 6.000   | .022               | . 022          | 6.000          | 4.000          | . 022    | 0 |
|                | B.D.                                    | K (CM) RHO(OHM-CM) R-SGR(OHM) VOC (MV) | .022               | .000    | .000               | .000           | .000           | .000           | . 000    |   |
|                | A.D.                                    | R-SOR(OHM)                             | 58.010             | 57.163  | 52.118             | 55.064         | .000           | 56.650         | 55.517   |   |
|                | AMO                                     | VOC (MV)                               | 549.000            | 546.000 | 544.000            | 533.000        | .000           | 538.000        | .000     |   |
|                | MILL                                    | ISC (NA)                               | 127.000            | 245.000 | 239.000            | 245.000        | .000           | 126.000        | .000     |   |
| and the second |   | VMP (MV)                               | 119.000            | 226.000 | 214.000            | 192.000        | .000           | 104.000        | .000     | - |
|                |   | FILL FCTR                              | .758               | .759    | .686               | .626           | .000           | .669           | .000     |   |
|                |   | EFFICIENCY                             | . 098              | .125    | .110               | .101           | .000           | . 084          | .000     |   |
|                | 1119                                    | VCC (NV)                               | 548.000            | 545.000 | 544.000            | 531.000        | .000           | 537.000        | . 000    |   |
|                |   | ISC (MA)                               | 111.000            | 213.000 | 206.000            | 213.000        | .000           | 109.000        | .000     |   |
|                |   | IMP (MV)                               | 453.000            | 453.000 | 190.000            | 425.000        | .000           | 69.000         | .000     |   |
|                |   | FILL FCTR                              | .760               | .765    | .704               | .594           | .000           | .662           | .000     |   |
|                |   | EFFICIENCY                             | .116               | .148    | .131               | .112           | .000           | 1.155          | .000     |   |
|                |   | EFF/AMO EFF                            | 1.163              | 1.184   | 1.198              | 1.111          | .000           | 1.155          | .000     |   |
|                |   |  |                    |         |                    |                |                |                | _        |   |
|                | WHEN                                    | BROKEN                                 | 0                  | 0       | 0                  | 0              | PROBE TES      | 0 7            | PRINTING |   |
|                |   |  |                    |         |                    |                |                |                |          |   |
|                |   |  |                    |         |                    |                |                |                |          |   |
|                | CELL                                    | NAME                                   |                    |         |                    | c              | D              | E E            | E        |   |
|                |   |  |                    |         |                    |                |                |                |          |   |
|                | AREA                                    | (CM2)                                  | 6.000              | 6.000   | 6.000              | 6.000          | 6.000          | 6.000          | 6.000    | - |
|                |   | K (CM)                                 | . 022              | .025    | . 025              | . 025          | . 025          | .025           | . 025    |   |
|                | E.D.                                    | RHO(OHM-CM)                            | 0.0.0              | .000    | .000               | .000<br>53.704 | .000<br>55.744 | .000<br>55.744 | .000     |   |
|                | A.D.                                    | R-SGR(OHM)                             | 52.931<br>544.000  | 51.665  | 55.517             | 528.000        | 526.000        | 530.000        | 526.000  | - |
|                |   | VOC (MV)                               |                    | .000    | 247.000            | 246.000        | 251.000        | 253.000        | 244.000  |   |
|                |   | VMP (MV)                               | 447.000            | .000    | 427.000            | 422.000        | 414.000        | 426.000        | 423.000  |   |
|                |   | IMP (MA)                               |                    | .000    | 226.000            | 226.000        | 231.000        | 235.000        | 226.000  |   |
|                |   | FILL FOTR                              | .747               | .000    | .737               | .734           | .724           | .747           | .745     |   |
|                |   | EFFICIENCY _                           | .121               | .000    | .119               | 527.000        | 525.000        | 529.000        | 525.000  |   |
|                |   | VOC (MV)                               | 543.000<br>209.000 | .000    | 529.000<br>215.000 | 213.000        | 218.000        | 219.000        | 214.000  |   |
|                |   | VMP (MV)                               | 445.000            | .000    | 425.000            | 426.000        | 419.000        | 429.000        | 424.000  |   |
|                |   | IMF (MA)                               | 189 000            | .000    | 195.000            | 194.000        | 199.000        | 202.000        | 195.000  |   |
|                |   | FILL FOTR                              | .741               | .000    | .729               | .736           | .729           | .748           | .736     |   |
|                |   | EFFICIENCY<br>EFF/AMC EFF              | 1.157              | .000    | 1.162              | 1.172          | 1.180          | 1.171          | 1.170    |   |
|                |   | Erry And Err                           |                    |         | .,,,               |                |                |                |          |   |
|                | NHEN                                    | EROKEN                                 | C .                | LOADING | CHIPPED            | CHIPPED        | CHIP/OHM       | IC 0           | CHIFPED  |   |
|                |   |  |                    |         |                    |                |                |                |          |   |
|                |   |  |                    |         |                    |                |                |                |          |   |
| 100            | CELL                                    | NAME                                   | с                  | ×1      | ×10                | X11            | X12            | X13            | X14      |   |
|                | 605                                     | (Cf(2)                                 | 6.000              |         |                    |                |                |                |          |   |
|                |   | K (CM)                                 | . 027              | 6.000   | 4.000              | 4.000          | 6.000          | 4.000          | . 627    |   |
|                |   | RHO( OHM-CM )                          | .000               | .000    | . 000              | .000           | .000           | . 000          | .000     |   |
|                |   | R-SURCOHM)                             | 58.010             | 46.226  | 48.946             | 49.852         | 48.492         | 48.492         | 45.093   |   |
|                |   | VOC (MV)                               | 531.000            | 59€.000 | 592.000            | 596.000        | 513.000        | 565.000        | 608.000  |   |
|                |   | ISC (MA)                               | 253.000            | 270.000 | 141.606            | 140.600        | 274.000        | 141.000        | 144.000  |   |
|                |   | IMP (MA)                               | 408.000            | 480.000 | 109.000            | 93.000         | 204.000        | 410.000        | 495.000  |   |
|                | * | FILL FOTE                              | .699               | .737    | .589               | .527           | .463           | 79.000         | 124.000  |   |
|                |   | EFFICIENCY                             | .116               | .147    | . 091              | . 080          | . 060          | . 060          | .113     |   |
|                | IMA                                     | VOC (MV)                               | 530.000            | 596.000 | . 000              | .000           | .000           | . 600          | 605.000  |   |
|                |   | ISC (MA)                               | 220.000            | 235.000 | .000               | .000           | .000           | . 600          | 124.000  |   |
|                |   | VMP (MV)                               | 416.000            | 480.000 | .000               | .000           | .000           | .000           | 496.000  |   |
|                | Sec. 1                                  | ******                                 | 198.000            | 217.000 | .000               | .000           | .000           | . 000          | 164.000  |   |
|                | AMI                                     | FILL ECTS                              | 704                | 744     | 0.0.0              |                |                |                |          |   |
|                |   | FILL FOTR<br>EFFICIENCY                | .706               | .744    | .000               | .000           | .000           | . 000          | .688     |   |

## Table 1 continued

|                |                                 | RESISTIVITY        | AND ILLUNIA    | NATED CHARA | CTERISTICS |         |         |                    |
|----------------|---------------------------------|--------------------|----------------|-------------|------------|---------|---------|--------------------|
|                |                                 |                    | uer.           | 801         |            |         |         |                    |
|                |                                 |                    |                |             |            |         |         |                    |
|                |                                 |                    |                |             |            | m + con |         |                    |
|                | CELL HAME                       | x2                 | ж3             | 84          | ×5         | ×6      |         | ×e                 |
|                |                                 |                    |                |             |            |         |         |                    |
| 305 100 0000 0 | AREA (CM2)                      | .000               | 6.000          | 6.000       | . 024      | 4.600   | 4.000   | 6.000              |
|                | B.D. RHO( OHM-CM )              | . 000              | .000           | .000        | 50.758     | .000    | 46.453  | .000               |
|                | A.D.R-SQR(OHM)                  | 597.000            | 51 . 212       | 51.212      | 604.000    | 596.000 | 496.000 | 599.000            |
|                | AMO ISC (MA)                    | 259.600            | .000           | .000        | 276.000    | 138.000 | 140.000 | 271.000            |
|                | AMO VMP (MV)                    | 495.000            | .000           | .000        | 244.000    | 130.000 | 71.000  | 459.000            |
|                | AMO FILL FOTE                   | .727               | .000           | .000        | .751       | .778    | .270    | .690               |
|                | AMO EFFICIENCY                  | .136               | ,000           | .000        | .151       | .119    | . 035   | . 138              |
|                | AMI VOC (MV)                    | .000               | .000           | .000        | 235.000    | 118.000 | .000    | 598.000<br>234.000 |
|                | AM! VMP (HV)                    | .000               | .000           | .000        | 496.000    | 496.000 | . 000   | 466.000            |
|                | AMI IMP (MA)                    | . 600              | .000           | .000        | 210.000    | 110.000 | .000    | 210.000            |
|                | AMI FILL FOTE<br>AMI EFFICIENCY | .000               | . 000          | .000        | .737       | .776    | .000    | .693               |
|                | AM1 EFF/AMO EFF                 | .000               | .000           | .000        | 1.151      | 1.149   | .000    | 1.182              |
|                | WHEN BROKEN                     | 0                  | TEMP. TEST     | 75 NO 7557  |            | 0       |         | 0                  |
|                | SHEN BRUKEN                     | U                  | TEMP. TEST     | IERP. IEST  | ·          | U       |         | •                  |
|                |                                 |                    |                |             |            |         |         |                    |
|                |                                 |                    |                |             |            |         |         |                    |
|                |                                 |                    |                |             |            |         |         |                    |
|                | CELL NAME                       | ×9                 | -              |             |            |         |         |                    |
| - 1            | AREA (CM2)                      | 4.000              |                |             |            |         |         |                    |
|                | THICK (CM)<br>B.D.RHO(GHM-CM)   | .000               |                |             |            |         |         |                    |
|                | A.D. K-SOR(OHM)                 | 53.704             |                |             |            |         |         |                    |
|                | AMO VOC (MV)                    | 599.000            |                |             |            |         |         |                    |
|                | AMO ISC (MA)                    | 146.000<br>456.000 |                |             |            |         |         |                    |
| * *            | AMO IMP (MA)                    | 121.000            |                |             |            |         |         |                    |
|                | AMO FILL FOTE                   | .642               |                |             |            |         |         |                    |
|                | AMO EFFICIENCY _                | . 102              |                |             |            |         |         |                    |
|                | AM: 150 (MA)                    | .000               |                |             |            |         |         |                    |
|                | AMI VMP (MV)                    | .600               |                |             |            |         |         |                    |
|                | AMI IMP (MA)                    | .000               |                |             |            |         |         |                    |
|                | AMI EFFICIENCY                  | .000               |                |             |            |         |         |                    |
|                | AM1 EFF/AMO EFF                 | .000               |                |             |            |         |         |                    |
|                |                                 |                    | Tabl           | le 2        |            |         |         |                    |
|                |                                 |                    | SPECTRAL SE    | ENSITIVITY  |            |         |         |                    |
|                |                                 |                    | UE             |             |            |         |         |                    |
|                |                                 |                    |                |             |            |         |         |                    |
|                |                                 |                    | The Section of |             |            |         |         |                    |
|                | CELL NAME                       | 1                  | 2              | 3           | 4          | 5       | 6       | ?                  |
|                | W.L. (MICRON)                   |                    |                |             |            |         |         |                    |
|                |                                 |                    |                |             |            | .000    | .127    | .000               |
|                | .41                             | .125               | .150           | .146        | .160       | .000    | .298    | .000               |
|                | .50                             | .394               | .451           | .437        | .456       | .000    | . 391   |                    |
|                | .55                             | .428               | .493           | .480        | .505       | .000    | .425    | .000               |
|                | .65                             | .462               | .521           | .556        | .560       | .000    | .459    | .000               |
|                | .70                             | .487               | .580           | .570        | .578       | .000    | .476    | .000               |
|                | .75<br>.80                      | .508               | .614           | .615        | .606       | .000    | .507    | . 000              |
|                | .85                             | .466               | .602           | .563        | .588       | . 000   | .476    | .000               |
|                | .90                             | .451               | .536           | .520        | . 556      | .000    | .479    | .000               |
|                | 1.05                            | . 098              | .126           | .116        | .120       | .000    | . 339   | . 000              |
|                | 1.05                            | . 070              |                |             |            |         |         |                    |

## Table 2 continued

SPECTRAL SENSITIVITY

| W.L. (MICRON)         |              | A     |       | c            | D     |       |       |   |
|-----------------------|--------------|-------|-------|--------------|-------|-------|-------|---|
| and the second second |              |       |       |              |       |       |       |   |
| .41                   | .154         | .000  | .152  | .149         | .157  | .148  | . 143 |   |
| .50                   | .450         | .000  | .442  | .430         | .460  | .452  | .439  |   |
| .55                   | .494         | .000  | .484  | .483         | .500  | .493  | .483  |   |
| .60                   | .520         | .000  | . 531 | . 526        | .547  | .542  | .523  |   |
| .65                   | .551         | .000  | .556  | .564         | .599  | .570  | .576  |   |
| .75                   | .600         | .000  | .614  | .616         | .628  | .622  | .611  |   |
| ,60                   | 591          | .000  | . 363 | .649         | . 654 | .657  | .639  |   |
| .65                   | .508         | .000  | .618  | .622         | .632  | . 636 | .618  |   |
| . 95                  | .547         | .000  | .560  | . 566        | .566  | .572  | .565  |   |
| 1.05                  | 121          | .000  | .137  | . 139        | .137  | .142  | .136  |   |
|                       |              |       |       |              |       |       |       |   |
| CELL NAME             | G            | X1    | X10   | ×11          | X12   | ×13   | X14   |   |
| W.L. (MICRON)         |              |       |       |              |       |       |       |   |
| .41                   | .152         | .146  | .162  | .206         | .167  | .246  | .147  |   |
| .45                   | .342         | .328  | .325  | .349         | .342  | .377  | .294  |   |
| .50                   | .450         | .503  | 407   | 413          | 445   | .423  | .407  | - |
| .60                   | .541         | .558  | .488  | .446         | .502  | .456  | .435  |   |
|                       | 571          | .592  | .496  | .487         |       | .492  | .485  |   |
| .76                   | .593         | .626  | .536  | .540         | .623  | .568  | .520  |   |
| . 80                  | .632<br>.648 | .704  | .894  | .573<br>.594 | .677  | .608  | .564  |   |
| .85                   | .644         | .743  | .637  | .623         | .767  | .645  | .632  |   |
| .90                   | .660         | .735  | .725  | .719         | .803  | .765  | .661  |   |
| 1.05                  | .476         | .702  | .357  | .659         | .650  | .746  | .710  |   |
|                       | . 140        | . 300 | .357  | .347         | .436  | .411  | .353  |   |
|                       |              |       |       | -            |       |       |       |   |
| CELL NAME             | ×2           | жз    | X4    | ×5           | ×6    |       | ×6    |   |
| W.L. (MICRON)         |              |       |       |              |       |       |       |   |
| .41                   | .161         | .000  | .000  | .165         | .127  | .344  |       |   |
| .45                   | . 331        | . 000 | .000  | .335         | .280  | .472  | . 166 |   |
| . 50                  | .437         | .000  | .000  | .445         | .390  | .453  | .460  |   |
| .60                   | .486         | .000  | .000  | .489         | .432  | .475  | .515  | - |
| . 65                  | 574          | . 000 | .000  | .545<br>.578 | .466  | .503  | .564  |   |
| .70                   | .613         | .000  | .000  | .622         | .511  | .624  | .634  |   |
| .75                   | .653         | .000  | .000  | .662         | .543  | .630  | .682  |   |
| .85                   | .742         | .000  | .000  | .707         | .569  | .622  | .716  |   |
| .90                   | .764         | .000  | .000  | .758         | .601  | .644  | .772  |   |
| .95                   | .776         |       | .000  | . 600        | .564  | .663  | .625  |   |
| 1.05                  | . 394        | .000  | .000  | .401         | .233  | .415  | 416   |   |
|                       |              |       |       |              |       |       |       |   |
| CELL NAME             | ×9           |       |       |              |       |       |       |   |
| W.L. (MICRON)         |              |       |       |              |       |       |       |   |
| .41                   | .160         |       |       |              |       |       |       | - |
| . 45                  | .316         |       |       |              |       |       |       |   |
| .55                   | .444         |       |       |              |       |       |       | - |
| . 60                  | .463         |       |       |              |       |       |       |   |
| .70                   | .518         |       |       | -            |       |       |       |   |
| .75                   | .518         |       |       |              |       |       |       | - |
|                       | 584          |       |       |              |       |       |       |   |
| . 65                  | .622         |       |       |              |       |       |       | - |
| . 90                  | .674         |       |       |              |       |       |       |   |
| 1.65                  | .336         |       |       |              |       |       |       |   |

Table 3

# RESISTIVITY AND ILLUMINATED CHARACTERISTICS CELL NAME 1 1 12

|     | HEN BROKEN        | DICING SAM | LOADING | 0       | 0       | SPEC . RESP | 0       | DICING SAU |
|-----|-------------------|------------|---------|---------|---------|-------------|---------|------------|
| * / |                   |            |         |         |         |             |         |            |
|     | MI EFF/AND EFF    | .000       |         | 1.173   |         | 1.177       |         |            |
|     | MI EFFICIENCY     |            |         | .132    |         |             |         | 000        |
|     | MI FILL FOTE      | .006       | .000    | .737    | .736    | .740        | .741    | .000       |
|     | MI IMP (Me)       | . 665      | .000    |         | 112.000 | 113.006     | 112.000 | .000       |
|     | MI VMP (MV)       | .000       | .000    | 470.000 |         | 468.000     |         | . 600      |
| -   | MI ISC (MA)       | .000       | .000    |         | 122.000 |             | 122.000 | .000       |
|     | MI VOC (MV)       | .000       | .000    | £75.000 | .109    |             | 575.000 | .000       |
|     | MG FILL FOTR      | .000       | .000    | .746    | .737    | .724        | .732    | .000       |
|     | MO IMP (MA)       | .000       | .000    |         |         | 131.000     | 130.000 | .000       |
|     | MO VMF (MV)       | .000       | . 000   |         | 457.000 |             |         | .600       |
|     | MO ISC (MA)       | .000       | .000    |         |         |             | 142.000 | .000       |
|     | MO VOC (MV)       | .060       | .000    | 580.000 |         | 563.000     | 578.000 | .000       |
|     | .D.R-SOR. OHM)    |            |         |         |         | 48.039      |         | .000       |
|     | D. RHO ( OHM-CM ) | 13.835     | 15.374  | 13.562  | 12.554  | 14.214      | 13.420  | 14.706     |
|     | HICK (CH)         | .018       | .018    | .016    | .010    | .018        | .018    | .018       |
|     |                   |            | 4.000   |         |         |             | 4.000   | 4. one     |
|     | ELL NAME          | . 2        | 3.      | 4       | 4       |             | 5,-     |            |
|     |                   |            |         |         |         |             |         |            |
|     | HEN BROKEN        | EDGE CLEAN | 0       | o       | 0       | SPEC . RESP | . 0     | 0          |
| •   | AM: EFF/AMO EFF   | .000       | 1.181   | .000    | 1.176   | 1.162       | .000    | 1.176      |
|     | AMI EFFICIENCY    |            | .129    |         | .125    |             |         | .133       |
|     | AMI FILL FOTR     | .000       | .734    | .000    | .736    | .754        | .000    | .742       |
|     | AMI IMP (MA)      |            | 112.000 | .000    | 111.000 |             | .000    | 114.000    |
|     | AMI VMP (MV)      |            | 462.000 | .000    | 450.000 |             |         | 466.000    |
|     | AM! ISC (MA)      | .000       | 123.000 | .000    | 121.000 | 123.000     | .000    | :23.000    |
|     | AMI VOC (MV)      | .000       | 573.000 | .000    | 561.000 | 580.000     | .000    | 592.000    |
|     | AND EFFICIENCY    |            |         | . 097   |         |             | 103     |            |
|     | AMO FILL FOTE     | .000       | .728    | .681    | .730    | .737        | .732    | .745       |
|     | AMO IMP (MA)      | .000       | 128.000 | 117.000 | 130.000 | 130.000     | 127.000 | 131.000    |
|     | AMO VMP (MV)      | .000       | 463.000 |         |         |             | 138.000 | 141.000    |
|     | And ISC (MA)      | .000       | 142.000 | 136.000 | 562.000 | 565.000     | 553.000 | 565.000    |
|     | ANO V. (NV)       | 49.652     | 47.586  |         |         |             | 46.680  | 47.133     |
|     | B.D.RHOKOHM-CM)   | 14.315     | 14.508  | 14.206  | 13.046  | 14.935      | 12.063  | 15.556     |
|     |                   |            |         |         |         |             |         |            |
|     | THICK (CH)        | .016       | .018    | .018    | .018    | .016        | .018    | .018       |

| CEL   | L NAME       | 6.      | •       |         | ٠         | •.      | ,       | *.     |
|-------|--------------|---------|---------|---------|-----------|---------|---------|--------|
| AFE   | A (CM2)      | 4.000   | 4.000   | 4.000   | 4.000     | 4.000   | 4.000   | 4.000  |
| THI   | CK (CM)      | .018    | .018    | .018    | .018      | .018    | .016    | .018   |
| B . D | RHO( OHM-CM) | 13.231  | 14.359  | 12.997  | 15.048    | 13.320  | 14.097  | 12.296 |
| A.D   | .R-SQR(OHM)  | 47.586  | 50.305  | 47.133  | 47.133    | 45.773  | 49.852  | 45.773 |
| AMO   | VOC Chirs    | 561.000 | 584.000 | 575.000 | 581.000   | 571.000 | 582.000 | .000   |
| AM 0  | ISC (MA)     | 141.000 | 144.900 | 127.000 | 142.000   | 140.000 | 139.000 | .000   |
| AMO   | VMP (MV)     | 436.000 | 471.000 | 461.000 | 469.000   | 455.000 | 471.000 | . 000  |
| AHO   | IMP (MA)     | 112.000 | 130.000 | 116.000 | 130.000   | 129.000 | 127.000 | .000   |
|       | FILL FOTR    | .620    | .728    | .732    | .739      | .734    | .739    | .000   |
|       | EFFICIENCY   | . 091   | .113    | . 099   | .113      | .108    | .111    | 000    |
|       | VOC (MV)     | .000    | 578.000 | .000    | 579.000   | 562.000 | 573.000 | . 000  |
| AMI   | ISC (MA)     | .000    | 124.000 | .000    | 122.000   | 122.000 | 121.000 | . 000  |
|       | VMP (MV)     | .000    | 470.000 |         | - 469.000 | 455.000 | 465.000 |        |
| AMI   | IMP (MA)     | .000    | 113.000 | .000    | 112.000   | 112.000 | 111.000 | .000   |
| AM I  | FILL FOTE    | .000    | .741    |         |           |         |         | . 000  |
|       |              |         |         | .000    | .744      | .743    | .744    | .000   |
|       | EFFICIENCY   | . 000   | .133    | . 000   | .131      | . 127   | .129    | .000   |
| AM1   | EFF/AMO EFF  | . 000   | 1.174   | . 000   | 1.166     | 1.175   | 1.167   | . 000  |

O EDGE ETCH O O 0 B.S.F.

WHEN BROKEN

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Table 3 continued

#### RESISTIVITY AND ILLUMINATED CHARACTERISTICS

|         |                | RESIS | TIVITY | AND ILLUMIN    | ATED CHARAC | CTERISTICS |         |           |         |        |
|---------|----------------|-------|--------|----------------|-------------|------------|---------|-----------|---------|--------|
|         |                |       |        | UEB            | 02          |            |         |           |         |        |
|         |                |       |        |                | •           |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
| 41.00.7 |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         | CELL HAME      |       |        | 13             | 13.         | 14         |         | 2         |         |        |
|         | CELL NAME      |       | 12.    | 13             |             | 1.4        |         | -         | •       |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         | AREA (CM2)     |       | .000   | 4.000          | 4.000       | 4.000      |         | 4.000     | 4.000   |        |
|         | THICK (CM)     |       | .018   | .018           | . 019       | .018       | .019    | .018      | .018    |        |
|         | B.D. PHOK OHM  |       | 2.127  | 15.209         | .000        | 14.613     | .000    | 13.706    | 14.291  |        |
|         | A.L.R-SORCO    |       | 5.773  | .000           | .000        | 48.492     | .000    | . 000     | 563.000 |        |
|         | AMO VOC CMV    |       | 7.000  | .000           | .000        | .000       | .000    | .000      | 140.000 |        |
|         | AND VMP (MV    |       | 7.000  | .000           | .000        |            |         | .000      | 472.300 |        |
|         | AMO IMP CHA    |       | 7.000  | .000           | .000        | .000       | .000    | .000      | 129.000 |        |
|         | AMO FILL FC    |       | .740   | .000           | .000        | .000       | . 600   | .000      | .746    |        |
|         | AMO EFFICIE    |       | .105   | .000           | .000        | .000       | .000    | .000      | .113    |        |
|         | AM1 VOC (MV    |       | .000   | .000           | .000        | .000       | .000    | .000      | 581.000 |        |
|         | ANT ISC (MA    |       | .000   | .000           | .000        | .000       | .000    | .000      | 122.000 |        |
|         | ANT VMP (MV    |       | .000   | .000           | .000        | .000       | .000    | . 000     | 112.000 |        |
|         | AMI IMP (MA    |       | .000   | .000           | .000        | .000       | . 600   | . 000     | .739    |        |
|         | AMI EFFICIE    |       | .000   | .000           | .000        | .000       | .000    | . 000     | 131-    |        |
|         | AM1 EFF/AMO    |       | .000   | .000           | .000        | .000       | .000    | .000      | 1.165   |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         | WHEN BROKEN    | 0     |        | V/I PROBE      | DICING      | V/I PROBE  | DICING  | SCRIB 1.0 | . 0     |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         | CELL HAME      |       | X1     | ×2             | ×3          | ×4         | ×5      | ×6        | ×7      |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         | 4.000     | 4 000   |        |
|         | AREA (CM2)     |       | .000   | 4.000          | 4.000       | 4.000      | .000    | . 023     |         |        |
|         | B.D. RHO! DHM  |       | .023   | . 023<br>1.948 | 2.031       | 1.989      | 2.196   | 2.134     | 2.002   |        |
|         | 4. D. R-SQR( 0 |       | 5.773  | 45.773         |             |            |         | 46 . 226  | 44.414  |        |
|         | AMO VOC (MV    |       | 0.000  | 603.000        | 313.000     | 576.000    | 598.000 | 601.000   | 605.000 |        |
|         | AND ISC (MA    |       | 7.000  | 149.000        | 137.000     | 146.000    | 149.000 | 142.000   | 152.000 |        |
| -       | AMO VMP (MV    |       | 0.600  | 509.000        | 178.000     | 437.000    | 495.000 | 498.000   | 504.000 |        |
|         | AMO IMP (MA    | ) 13: | 3.000  | 137.000        | 98.000      | 94.000     | 127.000 | 126.000   | 140.000 |        |
|         | AND FILL FC    | TR    | .754   | .776           | .407        | .488       | .706    | .735      | 767     |        |
|         | AMO EFFICIE    | NCY   | .123   | .129           | . 032       | . 076      | .116    | .116      | .130    |        |
|         | AMI VOC CHV    |       | . 600  | 601.000        | .000        | . 000      | .000    | .000      | 602.000 |        |
|         | AMI ISC (MA    |       | 7.000  | 129.000        | .000        | .000       | .000    | .000      | 502.000 | -      |
|         | AMI THE CMA    |       | . 000  | 120.000        | .000        | .000       | .000    | .000      | 122.000 |        |
|         | AMI FILL FC    |       | .744   | .762           | .000        | . 000      | .000    | .000      | .777    |        |
|         | AMI EFFICIE    | NCY   | .141   | .151           |             |            | 000     | . 000     | 153     |        |
|         | AM1 EFF/AMO    | EFF   | 1.146  | 1.176          | . 000       | .000       | . 660   | .000      | 1.174   |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        | _              |             |            |         |           |         |        |
|         | WHEN BROKEN    | ٥     |        | 0              | CELL SLIP   | 0          | 0       | c         | o       |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         | CELL NAME      |       | X8     |                |             |            |         |           |         | -      |
|         |                |       |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |
|         | AREA (CM2)     |       | . 900  |                |             |            |         |           |         |        |
|         | THICK (CM)     |       | . 023  |                |             |            |         |           |         |        |
|         | B.D. RHOCOHM   |       | . 634  |                |             |            |         |           |         |        |
|         | A.D.P-50R.0    |       |        |                |             |            |         |           |         |        |
|         | AMO VOC (MY    |       | 7.000  |                |             |            |         |           |         |        |
|         | AND VHP CHY    |       | 3.000  |                |             |            |         |           |         |        |
|         | AND IMP CHA    |       | 8.000  |                |             |            |         |           |         |        |
|         | AMO FILL FC    | TR    | .359   |                |             |            |         |           |         |        |
|         | AMO EFFICIE    |       | . 033  |                |             |            |         |           |         |        |
|         | AMI VOC CHY    | )     | . 660  |                |             |            |         |           |         |        |
|         | AMI ISC (MA    | )     | .000   |                |             |            |         |           |         |        |
|         | AMI VMP (MV    |       | .000   |                | -           |            |         |           |         |        |
|         | AMI IMP (MA    |       | .000   |                |             |            |         |           |         |        |
|         | AMI EFFICIE    |       |        |                |             |            |         |           |         |        |
|         | AMI EFF/AMO    |       | . 000  |                |             |            |         |           |         |        |
|         | e              | -     |        |                |             |            |         |           |         |        |
|         |                |       |        |                |             | ***        |         |           |         | 11,000 |
|         | WHEN BROKEN    | CHI   | P OHM  | C              |             |            |         |           |         |        |
|         |                |       |        |                |             |            |         |           |         |        |

Table 4

| CELL NAME   1  |               |       | SPECTRAL SE | HSTITIVITY |       |                                  |                                     |       |
|--|---------------|-------|-------------|------------|-------|----------------------------------|-------------------------------------|-------|
| U.L. (RICRON)  41  |               |       | . DEE       | 02         |       |                                  |                                     |       |
| ### #### #############################   |               |       |             |            |       | an distance and an electronic of |                                     |       |
| U.L. (MICRON)  41  |               |       |             |            |       |                                  |                                     |       |
| ### ### #### #########################   | CELL NAME     |       |             | 10         | 10.   | 11                               | 11.                                 | 12    |
| 45 000 225 227 236 241 250 244 55 26 254 37 374 364 65 255 260 0 349 345 363 347 374 364 65 55 000 433 422 445 444 449 443 445 15 0 000 479 468 495 493 466 462 15 000 528 596 595 577 556 555 555 75 000 659 539 577 556 555 555 75 000 628 600 000 614 610 630 662 553 620 553 620 600 600 600 614 610 630 662 553 620 553 620 600 600 710 668 642 702 609 600 900 6710 668 642 702 609 600 955 600 626 500 626 551 633 495 623 1.05 600 620 520 161 214 183 208   | W.L. (HICRON) |       |             |            |       |                                  |                                     |       |
| 45 000 225 227 226 241 250 244 55 24 35 347 374 364 65 255 200 00 342 345 363 347 374 374 364 65 55 000 479 468 495 493 466 462 55 000 526 596 597 576 556 555 555 75 000 625 599 577 556 555 555 75 000 625 599 577 556 555 555 75 000 625 599 577 556 555 555 75 000 625 599 577 556 555 555 75 000 625 599 577 556 555 555 75 000 625 599 600 000 634 610 630 620 593 620 593 600 600 600 710 668 644 700 600 649 90 000 710 668 644 700 600 600 625 591 621 633 499 623 1.05 000 620 200 202 161 214 183 208   | 41            |       | 097         | 498        | .099  | . 101                            | .105                                | .103  |
| 10   |               |       |             |            |       |                                  |                                     |       |
| . 1 0 000 .479 .468 .495 .493 .466 .482 .700 .000 .528 .506 .523 .524 .524 .524 .520 .70 .000 .528 .506 .523 .524 .524 .524 .520 .70 .000 .528 .509 .577 .556 .555 .555 .555 .555 .600 .60 .000 .625 .591 .621 .604 .553 .600 .80 .000 .604 .610 .630 .620 .533 .620 .90 .90 .000 .710 .668 .642 .702 .609 .620 .95 .000 .620 .655 .605 .649 .95 .000 .620 .655 .511 .633 .499 .623 .1.05 .000 .200 .202 .161 .214 .153 .208   |               |       | .349        | .345       | . 363 | .367                             |                                     |       |
| . 65   |               |       |             |            |       |                                  |                                     |       |
| .70  |               |       |             |            |       |                                  |                                     |       |
| 75 000 625 591 621 604 593 600 60 000 634 610 630 620 593 620 65 000 666 636 640 655 605 649 90 000 710 668 642 702 609 660 95 000 200 200 202 161 214 153 208  CELL NAME 3 3 4 4 5 5 5 6  W.L. (RICROH)  41 000 000 105 105 109 073 103 000 50 000 000 246 294 170 245 000 50 000 000 366 377 258 270 000 60 000 000 474 480 314 447 000 60 000 000 575 596 367 561 000 60 000 000 575 596 420 661 000 60 000 000 575 598 420 661 000 60 000 000 575 598 420 661 000 60 000 000 655 598 420 661 000 60 000 000 655 598 420 661 000 60 000 000 665 598 420 661 000 60 000 000 665 598 420 661 000 60 000 000 620 620 658 482 671 000 60 000 000 620 658 598 420 661 000 60 000 000 620 658 598 420 661 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 620 658 482 671 000 60 000 000 640 658 598 420 671 000 60 000 000 620 658 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 598 482 671 000 60 000 000 640 658 658 642 671 000 60 000 000 640 658 658 668 671 000 60 000 000 640 658 658 668 671 000 60 000 000 640 658 658 668 671 000 60 000 000 640 658 658 668 671 000 60 000 000 640 658 658 668 671 000 60 000 600 600 600 600 600 600 600  |               |       |             |            |       |                                  |                                     |       |
| 80 000 666 636 640 655 605 649 90 000 710 668 642 702 609 680 90 000 710 668 642 702 609 680 105 105 000 200 200 202 161 214 153 208 10.05 000 200 200 105 107 214 153 208 10.05 10. |               |       |             |            |       |                                  |                                     |       |
| 90 000 710 668 642 702 609 660  1.05 000 200 202 161 214 153 208  CELL NAME 3 3. 4 4. 5 5. 6  W.L. (MICROM)  (   |               |       |             |            |       |                                  |                                     |       |
| 1.05   |               | . 600 |             | .636       | .640  | .655                             |                                     |       |
| CELL NAME 3 3. 4 4. 5 5. 6  U.L. (RICROM)  .41 .000 .000 .105 .109 .073 .103 .000 .45 .000 .000 .248 .254 .170 .245 .000 .50 .000 .000 .366 .377 .258 .370 .000 .55 .000 .000 .472 .480 .314 .447 .600 .60 .000 .000 .575 .522 .363 .525 .000 .75 .000 .000 .575 .598 .416 .607 .000 .75 .000 .000 .575 .598 .416 .607 .000 .85 .000 .000 .575 .598 .416 .607 .000 .85 .000 .000 .575 .598 .416 .607 .000 .85 .000 .000 .575 .598 .416 .607 .000 .85 .000 .000 .575 .598 .416 .607 .000 .85 .000 .000 .575 .598 .410 .000 .95 .000 .000 .575 .598 .410 .000 .95 .000 .000 .575 .598 .420 .611 .000 .95 .000 .000 .575 .598 .420 .611 .000 .95 .000 .000 .575 .598 .420 .611 .000 .95 .000 .000 .520 .554 .417 .578 .000 .105 .000 .000 .562 .554 .417 .578 .000 .105 .000 .000 .562 .554 .417 .578 .000 .105 .000 .000 .187 .173 .140 .185 .000 .105 .000 .000 .187 .173 .140 .185 .000 .50 .321 .379 .241 .369 .393 .376 .000 .50 .321 .379 .241 .369 .393 .376 .000 .50 .321 .491 .445 .489 .496 .477 .000 .60 .491 .491 .445 .489 .496 .477 .000 .65 .526 .516 .478 .525 .523 .512 .000   |               |       |             |            |       |                                  |                                     |       |
| CELL NAME 3 3. 4 4. 5 5. 6  W.L. (MICRON)  41 .000 .000 .105 .109 .073 .103 .000 .45 .000 .000 .246 .254 .170 .245 .000 .50 .000 .000 .346 .377 .258 .370 .000 .60 .000 .000 .474 .480 .335 .456 .000 .60 .000 .000 .575 .526 .363 .525 .000 .70 .000 .000 .575 .554 .367 .561 .000 .70 .000 .000 .575 .598 .420 .611 .000 .80 .000 .000 .575 .598 .420 .611 .000 .85 .000 .000 .605 .598 .420 .611 .000 .85 .000 .000 .618 .626 .444 .641 .000 .95 .000 .000 .620 .625 .482 .671 .000 .95 .000 .000 .562 .554 .417 .578 .000 .1.05 .000 .000 .167 .173 .140 .165 .000 .50 .000 .000 .167 .173 .140 .165 .000 .50 .000 .000 .167 .173 .140 .165 .000 .50 .321 .379 .241 .369 .393 .376 .000 .50 .321 .379 .241 .369 .393 .376 .000 .50 .321 .491 .445 .89 .496 .477 .000 .60 .478 .526 .516 .478 .525 .523 .512 .000   |               |       |             |            |       |                                  |                                     |       |
| W.L. (RICRON)  41 000 000 105 109 073 103 000 45 000 000 246 254 170 245 000 50 000 000 366 377 258 370 000 55 000 000 476 480 315 496 000 60 000 000 476 480 335 496 000 65 000 000 587 522 363 525 000 70 000 000 587 522 363 525 000 75 000 000 575 598 416 607 000 60 000 000 575 598 420 611 000 65 000 000 605 598 420 611 000 65 000 000 605 598 420 611 000 65 000 000 618 626 444 641 000 69 000 000 620 659 482 671 000 95 000 000 562 554 417 578 000 1.05 000 000 187 173 140 165 000  CELL NAME 6 7 7 8 8 9 9  W.L. (RICRON)  CELL NAME 6 7 7 8 8 9 9  W.L. (RICRON)  41 113 110 094 105 144 106 000 60 301 379 741 369 393 376 000 60 491 491 491 445 489 496 477 000 65 526 556 556 556 476 555 523 512 000   | 1.05          | . 000 | .200        | . 202      | . 161 | .214                             | . 153                               | . 206 |
| ### L. (HICRON)  ### 1   |               |       |             |            |       |                                  |                                     |       |
| ### ### ##############################   | CELL NAME     |       | 3.          |            | 4,    | - 5                              | · · · · · · · · · · · · · · · · · · |       |
| ### ### ##############################   | W.L. (MICRON) |       |             |            |       |                                  |                                     |       |
| ### ### ##############################   | 41            | 666   | 0.00        | 105        | 109   | . 673                            | .103                                | .000  |
| S0   |               |       |             |            |       |                                  |                                     |       |
| SE   |               |       |             |            |       |                                  |                                     | .000  |
| .60  |               |       |             | .434       | .448  |                                  |                                     |       |
| .70  |               | .060  | .000        |            |       |                                  |                                     |       |
| 75   |               |       |             |            |       |                                  |                                     |       |
| CELL NAME  |               |       |             |            |       |                                  |                                     |       |
| SS   |               |       |             |            |       |                                  |                                     |       |
| CELL NAME 6. 7 7. 8 8. 9 9  W.L. (HICRON)  1.13 110 094 105 144 106 000  .41 113 110 094 105 144 106 000  .45 256 259 227 245 290 254 000  .50 381 379 341 369 393 376 000  .55 453 442 410 446 458 444 000  .60 491 491 445 489 496 477 000  .65 526 516 478 525 523 512 000  |               |       |             |            |       |                                  |                                     |       |
| 95   |               |       |             |            |       |                                  |                                     |       |
| CELL NAME 6. 7 7. 8 8. 9 9.  U.L. (MICRON)  .41 .113 .110 .094 .105 .144 .106 .000 .45 .256 .259 .227 .245 .290 .254 .000 .50 .381 .379 .741 .369 .393 .376 .000 .50 .453 .442 .410 .446 .458 .444 .000 .60 .491 .491 .445 .489 .496 .477 .000 .65 .526 .516 .478 .525 .523 .512 .000  |               |       |             |            |       |                                  |                                     |       |
| W.L. (MICRON)  .41   |               |       |             |            |       |                                  |                                     |       |
| W.L. (MICRON)  .41   |               |       |             |            |       |                                  |                                     |       |
| W.L. (MICRON)  .41   |               |       |             |            |       |                                  |                                     |       |
| .41 .113 .110 .094 .105 .144 .106 .000 .45 .256 .259 .227 .245 .290 .254 .000 .50 .361 .379 .741 .369 .393 .376 .000 .55 .453 .442 .410 .446 .458 .444 .000 .60 .491 .491 .445 .489 .496 .477 .000 .65 .526 .516 .478 .525 .523 .512 .000  |               | 6.    | 7           | 7.         |       | 8                                | ,                                   | 9.    |
| .45 .256 .259 .227 .245 .290 .254 .000 .50 .361 .379 .341 .369 .393 .376 .000 .55 .453 .442 .410 .446 .458 .444 .000 .60 .491 .491 .445 .469 .496 .477 .000 .65 .526 .516 .478 .525 .523 .512 .000   |               |       | 114         | 69.        | 105   | 144                              | . 106                               | .000  |
| .50 .381 .379 .241 .369 .393 .376 .000<br>.55 .453 .442 .410 .446 .458 .444 .000<br>.60 .491 .491 .445 .489 .496 .477 .000<br>.65 .526 .516 .478 .525 .523 .512 .000   |               |       |             |            |       |                                  |                                     |       |
| .55 .453 .442 .410 .446 .458 .444 .000<br>.60 .491 .491 .445 .489 .496 .477 .000<br>.65 .526 .516 .478 .525 .523 .512 .000   |               |       |             |            |       |                                  |                                     |       |
| .60 .491 .491 .445 .489 .496 .477 .000<br>.65 .526 .516 .478 .525 .523 .512 .000   |               |       |             |            |       |                                  | .444                                | .000  |
| .65 .526 .516 .478 .525 .523 .512 .000   |               |       |             | .445       | . +89 | .496                             |                                     |       |
| TA FAT BAS BAS BEA BAS BAS AAA   |               | .526  | .516        | .478       |       |                                  |                                     |       |
|  | .70           | .563  | .546        | .505       | .550  | .565                             | .529                                | . 600 |
| .75 .607 .564 .540 .606 .595 .564 .000   |               |       |             |            |       |                                  |                                     |       |
| .60 .614 .617 .544 .621 .592 .606 .000   |               |       |             |            |       |                                  |                                     |       |
| .85 .642 .638 .568 .653 .595 .629 .000<br>.90 .674 .650 .586 .691 .617 .654 .000   |               |       |             |            |       |                                  |                                     |       |
| .90 .674 .650 .586 .691 .617 .654 .000<br>.95 .580 .598 .504 .620 .49£ .594 .000   |               |       |             |            |       |                                  |                                     |       |
| 1.05 .189 .206 .165 .204 .172 .200 .000  |               |       |             |            |       |                                  |                                     |       |

Table 4 continued

## SPECTRAL SENSITIVITY

| CELL NAME     | 12.  | 13   | 13.  | 10   | 14.    | •      | •.   |
|---------------|------|------|------|------|--------|--------|------|
| W.L. (MICRON) |      |      |      |      |        |        |      |
| .41           | .115 | .000 | .000 | .000 | .000   | .000   | .110 |
| .45           | .272 | .000 | .000 | .000 | .000   | .000   | .261 |
| .50           | .389 | .000 | .000 | .000 | .000   |        | 332  |
| .55           | .451 | .000 | .000 | .000 | .000   | .000   | .448 |
| .60           | .483 | .000 | .000 | .000 | .000   | .000   | .480 |
| .65           | .510 | .600 | .000 | .000 | .000 - | .000   | .512 |
| .70           | .536 | .000 | .000 | .000 | .000   | .000   | .539 |
| .75           | .569 | .000 | .000 | .000 | .000   | .000   | .576 |
|               | .570 | 000  | .000 | .000 |        |        | 591  |
| . 05          | .586 | .000 | .000 | .000 | .000   | .000   | .619 |
| .90           | .596 | .000 | .000 | .000 | .000   | .000   | .639 |
| .95           | .479 | .000 |      |      | .000   | .000 - | .567 |
| 1.05          | .151 | .000 | .000 | .000 | .000   | .000   | .200 |

| CELL NAME     | X1   | ×2   | X3   | ×4   | ×5   | X6    | X7   |
|---------------|------|------|------|------|------|-------|------|
| W.L. (MICRON) |      |      |      |      |      |       |      |
| .41           | .105 | .106 | .112 | .115 | .126 | .111  | .109 |
| .45           | .241 | .242 | .234 | .261 | .267 | .232  | .248 |
| .50           | .365 | .368 | .339 | .363 | .383 | .347  | .376 |
| .55           | .441 | .446 | .406 | .452 | .459 | . 426 | .451 |
| .60           | .490 | .495 | .457 | .482 | .457 | .475  | .500 |
| .65           | .525 | .532 | .488 | .519 | .535 | .514  | .540 |
| .70           | .562 | .569 | .532 | .555 | .590 | .560  | .578 |
| .75           | .616 | .624 | .575 | .605 | .633 | .613  | .627 |
| .86           | .656 | .656 | .617 | .630 | .666 | .651  | .667 |
| .65           | .663 | .694 | .637 | .669 | .707 | .693  | .709 |
| .50           | .721 | .754 | .661 | .733 | .603 | .776  | .776 |
| .95           | .740 | .764 | .609 | .734 | .798 | .767  | .794 |
| 1.05          | .319 | .340 | .304 | .313 | .371 | .366  | .373 |

| CELL | HAME     | 88   |
|------|----------|------|
| u.L. | (MICRON) |      |
|      | .41      | .217 |
|      | .45      | .310 |
|      | .50      | .359 |
|      | .55      | .415 |
|      | .60      | .465 |
|      | .65      | .490 |
|      | .70      | .617 |
|      | .75      | .628 |
|      | .60      | .626 |
|      | .85      | .666 |
|      | . 9      | .911 |
|      | .95      | .715 |
|      | 1.05     | .369 |
|      |          |      |

Table 5

|  |  | WE(   | 603   |  |   |          |         |
|--|--|---|---|--|---|----------|---------|
| CELL NAME  | 175 1  | 176.3   | 167 1   | 191 1  | X1  | X2       | жз      |
| APEA (CM2)   | e.000  | 6.000   | 8.000   | 8.000  | 8.000   | 8.000    | 0.00    |
| THICK (CM)   | 027  | .025  | .024  | .028   | .030  | . 033    | . 63    |
| B.D. RHOCOHM-CM)   | . 1100   | .000  | .000  | .000   | .000  | .000     | .00     |
| A.D.R-SOR(OHM)   | 111,714  | 1 06.275  | 140.719   | 101.290  | 108.315   | 119.645  | 97.66   |
| AMO VOC (MV)   | 521.000  | 531.000   | 525.000   | 231.000  | 294.000   | 255.000  | 262.00  |
| AMO ISC (MA)   | 377.000  | 214.000   | 412.000   | 406.000  | 309.000   | 382.000  | 469.00  |
| AND IMP (MA)   | 220.000  | 198.000   | 234.000   | 223.000  | 221.606   | 189.000  | 260.00  |
| AMO FILL FOTR  | .663   | .718  | .729  | .735   | .477  | ,511     | .77     |
| AND EFFICIENCY   | . 077  | .075  | .089  | .084   | .063  | .067     | .11     |
| HHI VOC (MV)   | 523.000  | 532.000   | 525:000   | 533.000  |   |          | 584:00  |
| HITT 180 (MA)  | 204.000  | 182.000   | 215.000   | 209.000  | .000  | .000     | 242.00  |
| ANT VHP (NV)   | 377.000  | 421.000   | 416.000   | 419.000  | .000  | .000     | 486.00  |
| HM1 IMP (MH)   | 190.000  | 170.000   | 200.000   | 192.000  | .000  | .000     | .77     |
| AMI EFFICIENCY   | .090   | .089  | .104  | .101   | .000  | .000     | .13     |
| AMT EFF/AMO EFF  | 1.166  | 7.167   | 1.166   | T.202  |   |          | 7.15    |
| WHEN BROKEN  | RESISTIVITY  | EVAPORATOR  |   | CTERISTICS"  |   | BACKETCH | UNCOAD  |
|  |  | AND ILLUMI  |   | CTERISTICS"  |   | BACKETCH | UNLOAD  |
|  |  | AND ILLUMI  | HATED CHARA   | CTERISTICS"  | ×ė  | BACKETCH | UNICAD  |
| WHEN BROKEN  |  | AND ILLUMIN   | NATED CHARA<br>603<br>  | ×7<br>8.000  | X6<br>6.000   | BACKETCH | UNLOAD  |
| CELL NAME  MEE (CM2) THICK (CM)  | KESISTIVITY  K4  6.000  .030                                     | ##D   | NATED CHARA<br>603<br>  | 8.000<br>.023  | #6.000<br>.133  | BACKETCH | UNLOAD  |
| CELL NAME  HREA (CM2) THICK (CM) B.D. PHOLOHM-CM)  | #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #                         | ##D ILLUMIO<br>#E1<br>25<br>6.000<br>.030   | NATED CHARA<br>603<br>  | 8.000<br>.033  | #6.000<br>.033<br>.000  | BACKETCH | UNICAD  |
| CELL NAME  AREA (CM2) THICK (CM) B. D. PHOS CHM-CM) A. D. P-SOR CHM)   | #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #                         | ## ILLUMIN<br>## ## ## ## ## ## ## ## ## ## ## ## ##  | 8.000<br>- 030<br>- 030<br>- 000<br>- 91.773  | 8.000<br>.033<br>.000<br>61.123  | 6.000<br>.033<br>.000<br>79.990   | BACKETCH | UNICAD  |
| CELL NAME  MREA (CM2) THICK (CM) B.D. PHOLOHM-CM)  | #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #                         | #EI ILLUMII  #EI  #5  8.000  .030 .000 94.945 578.000   | NATED CHARA<br>603<br>  | 8.000<br>.033  | #6.000<br>.033<br>.000  | BACKETCH | UNICAD  |
| CELL NAME  HREA (CM2) THICK (CM) B.D.PHOLOHMO-CM) HMA VOC (MV) HMA VOC (MV) HMA VOC (MV) HMA VOC (MV)  | ## ## ## ## ## ## ## ## ## ## ## ## ##                           | ## ILLUMIN<br>## ## ## ## ## ## ## ## ## ## ## ## ##  | 8.000<br>8.000<br>91.773  | 8.000<br>.033<br>.000<br>61.123<br>567.000   | 8.000<br>.133<br>.000<br>79.990<br>561.000<br>274.000<br>444.000  | BACKETCH | UNICAD  |
| CELL NAME  HREA (CM2) THICK (CM) B.D.PHOLOHMO-CM) AMD VOC (MV) AMD VOC (MV) AMD VOC (MV) AMD THE (MA)  | #4<br>#4<br>#000<br>.030<br>.000<br>.000<br>.000<br>.000<br>.000 | #EI HEI HEI HEI HEI HEI HEI HEI HEI HEI H   | 8.000<br>91.773<br>586.000<br>167.000   | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000   | 6.000<br>.233<br>.000<br>79.990<br>561.000<br>274.000<br>444.000  | BACKETCH | UNLOAD  |
| CELL NAME  MREA (CM2) THICK (CM) B.D.PHOLOMM-CM) M.D.R-SOR OMM) MMO VOC (MV) MMO 15C (MA) AMO VMP (MV) AMO FILL FCTR   | ## ## ## ## ## ## ## ## ## ## ## ## ##                           | #EI ILLUMII  #EI  #5  8.000  .030 .000 94.945 576.000 264.000 463.000 263.000 .742                      | 8.000<br>   | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000  | 6.000<br>.233<br>.000<br>79.990<br>561.000<br>274.000<br>444.000<br>251.000   | BACKETCH | UNICAD  |
| CELL NAME  AREA (CM2) THICK (CM) B.D.P-SOR OHM AND VOC (MV) AND VOC (MV) AND VOC (MV) AND VOC (MV) AND THE (MA) AND THE (MA) AND THE (MA) AND FILL FCTR AND EFFICIENCY   | ## ## ## ## ## ## ## ## ## ## ## ## ##                           | ##D ILLUMIN ###  ###  ###  ###  ###  ###  ###  #  | 8.000<br>9.000<br>91.773<br>586.000<br>167.000<br>486.000<br>71.0   | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000<br>.697<br>.093                                  | 8.000<br>.233<br>.000<br>.79.990<br>561.000<br>274.000<br>444.000<br>.725<br>.103   | BACKETCH | UNICOAD |
| CELL NAME  AREA (CM2) THICK (CM) B.D.P-SOR OHM) AMO VOC (MV) AMO ISC (MA) AMO FILL FOTA AMO FILL FOT | #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #                         | ##D ILLUMIN  ##E  ##E  ##E  ##E  ##E  ##E  ##E  #   | 8.000<br>8.000<br>91.773<br>506.000<br>167.000<br>486.000<br>160.000<br>710<br>072  | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000<br>.697<br>.093<br>565.000                       | 8.000<br>.033<br>.000<br>.79.990<br>561.000<br>274.000<br>444.000<br>.725<br>.103   | BACKETCH | UNICAD  |
| CELL HAME  HREA (CM2) THICK (CM) B.D.PHOLOHMOON AMO VOC (MV) AMO THE (MH) AMO FILL FCTR AMO EFFICIENCY AMI VOC (MV) AMI ISC (MH) AMI ISC (MH)  | #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #4 #                         | #EI ILLUMII  #EI  #5  8.000  030  94.945  576.000  263.000  263.000  742  112  576.000  244.000         | 8.000<br>91.773<br>586.000<br>167.000<br>710<br>072<br>585.000<br>163.000   | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000<br>.697<br>.093<br>565.000<br>220.000            | 6.000<br>.133<br>.000<br>79.990<br>561.000<br>274.000<br>444.000<br>251.000<br>.725<br>.103<br>.563.030<br>234.000            | BACKETCH | UNICAD  |
| CELL NAME  PREA (CM2) THICK (CM) B.D.P-SOR OHM) AMO VOC (MV) AMO INC (MA) AMO FILL FOTE AMO EFFICIENCY AMI VOC (MV)   | ## ## ## ## ## ## ## ## ## ## ## ## ##                           | #EI ILLUMII  #EI  #5  8.000  .030 .000 94.945 576.000 264.000 463.000 .742 .112 576.000 244.000 471.000 | 8.000<br>8.000<br>0.30<br>0.00<br>91.773<br>586.000<br>167.000<br>466.000<br>710<br>0.72<br>585.000<br>163.000<br>499.000 | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000<br>.697<br>.693<br>565.000<br>220.000<br>450.000 | 6.000<br>.233<br>.000<br>79.990<br>561.000<br>444.000<br>444.000<br>251.000<br>.725<br>.103<br>563.000<br>234.000<br>449.000  | BACKETCH | UNICAD  |
| CELL NAME  AREA (CM2) THICK (CM, B.D.P-SOR OHM) AND VOC (MV) AND ISC (MA) AND VOC (MV) AND ISC (MA) AND INP (MA)   | ## ## ## ## ## ## ## ## ## ## ## ## ##                           | ##D ILLUMIN ####################################  | 8.000<br>91.773<br>586.000<br>167.000<br>486.000<br>160.000<br>163.000<br>489.000   | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000<br>.697<br>.093<br>565.000<br>220.000<br>134.040 | 86.000<br>.233<br>.000<br>79.990<br>561.000<br>444.000<br>444.000<br>.725<br>.103<br>563.030<br>234.000<br>449.000<br>213.000 | BACKETCH | UNLOAD  |
| CELL NAME  PREA (CM2) THICK (CM) B.D.P-SOR OHM) AMO VOC (MV) AMO INC (MA) AMO FILL FOTE AMO EFFICIENCY AMI VOC (MV)   | ## ## ## ## ## ## ## ## ## ## ## ## ##                           | #EI ILLUMII  #EI  #5  8.000  .030 .000 94.945 576.000 264.000 463.000 .742 .112 576.000 244.000 471.000 | 8.000<br>8.000<br>0.30<br>0.00<br>91.773<br>586.000<br>167.000<br>466.000<br>710<br>0.72<br>585.000<br>163.000<br>499.000 | 8.000<br>.033<br>.000<br>61.123<br>567.000<br>255.000<br>452.000<br>223.000<br>.697<br>.693<br>565.000<br>220.000<br>450.000 | 6.000<br>.233<br>.000<br>79.990<br>561.000<br>444.000<br>444.000<br>251.000<br>.725<br>.103<br>563.000<br>234.000<br>449.000  | BACKETCH | UNICOAD |

Table 6

#### SPECTRAL SENSITIVITY

NECO3

| ×e       | X7    | ×6   | ×5   | ×4   | CELL NAME     |
|----------|-------|------|------|------|---------------|
|          |       |      |      |      | W.L. (MICRON) |
| <br>.104 | 7.046 | .096 | .112 | .000 |               |
| .221     | .193  | .181 | .232 | .000 | .45           |
| .317     | .269  | .263 | .317 | .000 | .50           |
| <br>.361 | .341  | .322 | .350 | .000 | .55           |
| .419     | .392  | .358 | .435 | .000 | .60           |
| .457     | .427  | .368 | .405 | .000 | .65           |
| <br>471  | .466  | .415 | .511 | .000 | .76           |
| .503     | .494  | .444 | .542 | .000 | .75           |
| .544     | .533  | .474 | .577 | .000 | .80           |
| <br>.544 | .566  | .483 | .600 | .000 | .05           |
| .527     | .566  | .496 | .609 | .000 | .90           |
| .498     | .548  | .497 | .605 | .000 | .95           |
| <br>.186 | 226   | .203 | .247 | .000 | 1.05          |

#### SPECTANL SEMBITIVITY

WE003

| CELL NAME     | 175 1 | 175 3 | 167 1 | 191 1 | X1   | ×2   | х3   |
|---------------|-------|-------|-------|-------|------|------|------|
| W.L. (MICRON) |       |       |       |       |      |      |      |
| .41           | .095  | . 663 | .107  | . 093 | .124 | -112 | .113 |
| .45           | .207  | .172  | .217  | .167  | .262 | .246 | .236 |
| .50           | .298  | .245  | .311  | .272  | .334 | .321 | .325 |
| .55           | .354  | .308  | .369  | .345  | .410 | .376 | .401 |
| .60           | .367  | .350  | .411  | .386  | .454 | .425 | .449 |
| .65           | .417  | .362  | .435  | .416  | .496 | .457 | .475 |
| .70           | .432  | .404  | .456  | .437  | .522 | .465 | .5.3 |
| .75           | .451  | .419  | .464  | .458  | .550 | .522 | .521 |
| .00           | .466  | .420  | .476  | .470  | .577 | .562 | .54? |
| .65           | .456  | .410  | .473  | .466  | .609 | .577 | 572  |
| .90           | .409  | .376  | .428  | .421  | .614 | .580 | .566 |
| .95           | .324  | .285  | .320  | .322  | .608 | .573 | .554 |
| 1.05          | .095  | .063  | .091  | .096  | .259 | .250 | .218 |

Table 7

|                                   |         | EF        | .02       |         |          |              |         |
|-----------------------------------|---------|-----------|-----------|---------|----------|--------------|---------|
| CELL NAME                         | A1      | A2        | A3        | n4      | A5       | A6           | A7      |
| AREA (Ch2)                        | 6.450   | 6.450     | 6.450     | 6.450   | 6.450    | 6.450        | 6.450   |
| THICK (CH)                        | .037    | .032      | . 039     | .038    | .034     | .030         | . 627   |
| B.D.RHO(OHM-CM)<br>A.D.R-SOR(OHM) | 2.136   | 1.338     | 1.766     | 1.425   | 1.904    | 47.359       | 52.798  |
| AMO VOC (MV)                      | .000    |           | .000      | .000    | .000     | 000          | .000    |
| and ISC (MA)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AND VMP (MV)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMO FILL FCTR                     | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AND EFFICIENCY                    | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| ANT VOC (MV)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI VMP (MV)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI IMP (Mm)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI FILL FOTR                     | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI EFFICIENCY                    | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
|                                   |         |           |           |         |          |              |         |
| WHEN BROKEN                       | DICING  | BHCK ETCH | PRINTING  | SPINNER | PRINTING | PRINTING     | HEL BOT |
| CELL NAME                         | #9      | A9        | 61        | 62      | 63       | 64           | 65      |
| AREA (CM2)                        | 6.450   | 6.450     | 6.450     | 6.450   | 6.450    | 6.450        | 6.450   |
| THICK (CH)                        | .026    | .034      | .036      | .036    | .037     | .036         | .033    |
| B.D. RHOCOHM-CH >                 | .000    | 2.642     | 1.338     | 1.644   | 1.579    | 1.330        | 1.661   |
| H.D.R.SOR(OHM)                    | .000    | 55.517    | 46.000    | 48.946  | 48.719   | 49.172       | 48.946  |
| AMO VOC (MV)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMO VMP (MV)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AND IMP (NA)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AND FILL FOTE                     | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMO EFFICIENCY                    |         | 000       |           | .000    | .000     | .000         | .000    |
| AMI ISC (MA)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| Ant VMF (MV)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI INF (MA)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| ANT EFFICIENCY                    | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI EFFZAMO EFF                   | .000    |           | 000       | .000    |          |              | . 000   |
| UHEN BROKEN                       | БІСТНЕ  | BHCK ETCH | BACK EYCH | SHISTO  | FIRTHS   | -растис      | V/I PRO |
|                                   |         |           |           |         |          |              |         |
| CELL NAME                         |         | _67       | E0        | 69      | <u> </u> | . <u>ç</u> 2 | c3      |
| AREA (CM2)                        | 6.450   | 6.450     | 6.450     | 6.450   | 6.450    | 6.450        | 6.450   |
| THICK (CH)                        | .030    | . 025     | .029      | 1.395   | 1.464    | 1.763        | 1.562   |
| A.D.R-SOR OHM                     | 1.265   | 1.197     | .000      | 51.691  | 48.206   | 49.172       | 48.039  |
| HHO VOC (MV)                      | 473.000 |           | :000      | 000     | .000     | 000          | 000     |
| AMO ISC (MA)                      | 139.000 | .000      | .000      | .000    | .000     | .000         | .000    |
| AND VER CHY)                      | 72.000  |           | .000      | .000    | .000     | .000         | .000    |
| AMO FILL FOTR                     | .300    | .000      | .000      | .000    | .000     | ,000         | .000    |
| AND EFFICIENCY                    | ,029    | .000      | .000      | .000    | .000     | .000         | .000    |
| HILL VOC (NV)                     | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI ISC (MA)                      | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI IMP (MA)                      | .,000   | 000       |           | .000    | .000     |              | .000    |
| AMI FILL FCTR                     | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| AMI EFFICIENCY                    | .000    | .000      | .000      | .000    | .000     | .000         | .000    |
| TOME PERSONS PER                  | A A A   | 0.00      | 0.00      | 0.00    | 41,1111  | . 11 (1 1)   |         |
| AMT EFF/AMO EFF                   | .000    | .000      | 000       | . 000   |          |              | .000    |

## Table 7 continued

| /                                 | ****      | *         | G02                |          |           |           |        |
|-----------------------------------|-----------|-----------|--------------------|----------|-----------|-----------|--------|
| CELL NAME                         | C4        | ce.       |                    | 67       | Ce .      | C9_       | 002    |
|                                   | 6.450     | 6.450     | 6.450              | 6.450    | 6.450     | 6.450     | 6.45   |
| THICK (CM)                        | .037      | .032      | .029               | .025     | .628      | . 633     | . 03   |
| B.D.RHO(OHM-CM)                   | 1.360     | 1.343     | 1.357              | 1.635    | 1.486     | 1.399     | 49.85  |
| A.D.R-SOR(OHM)                    | 48,719    | 47.359    | 52.116             | 52.116   | 353.000   | .000      | 478.00 |
| AND VOC (MV)                      | .000      | .000      | .000               | .000     | 140.000   | .000      | 136.00 |
| AMO VMP (MV)                      | .000      | .000      | .000               | .000     | 195.000   | .000      | 368.00 |
| AMO IMP (MH)                      | .000      | .000      | .000               | .000     | 75.000    | .000      | .54    |
| AMO FILL FOTR                     | .000      | .000      | .000               | .000     | .017      | .000      | .04    |
| AND EFFICIENCY                    |           | 000       |                    | 000      | .000      | :000      | .00    |
| AM1 ISC (MH)                      | .000      | .000      | .000               | .000     | .000      | .000      | .00    |
| AMI VIP (NV)                      | .000      | 000       | 000                |          | .000      | :000      | .00    |
| AMI IMP (MA)                      | .000      | .000      | .000               | .000     | .000      | .000      | .00    |
| AMI EFFICIENCY                    | .000      | .000      | .000               | .000     | .000      | .000      |        |
| HMT EFF/HMO EFF                   |           | .000      | . 000              | .000     | . 600     | .000      | .00    |
| WHEN EROKEN                       | SPINNER   | FIRING AL | SPINNER            | PRINTING |           | SPINNER   |        |
| CELL NAME                         | D1        |           | 63                 | 04       | 0.5       | . (·é     | 07     |
|                                   |           |           |                    |          |           |           |        |
| AREA (CM2)                        | 6.450     | 6.450     | 6.450              | 6.450    | 6.450     | 6.450     | 6.45   |
| THICK (CM)                        | .034      | .032      | . 634              | 1.279    | 1.907     | 1.865     | .00    |
| B.D.RHOKOHM-CM)<br>A.D.R-SORKOHM) | 1.376     | 49.852    | 1.608              | 49.852   | .000      | .000      | .00    |
| AMO VOC (MV)                      | .000      | 478.000   | .000               | .000     | -:000     | .000      | .00    |
| Amo ISC (MA)                      | .000      | 136.000   | .000               | .000     | .000      | .000      | .00    |
| AND VMP (NV)                      | .000      | 96.000    | .000               | .000     | .000      | .000      | .00    |
| AMO FILL FOTE                     | .000      | .543      | .000               | .000     | .000      | .000      | .00    |
| AND EFFICIENCY                    | .000      | .040      | .000               | .000     | .000      | .000      | .00    |
| AMI VUC (MY)                      | .000      | .000      | . 600              | .000     | .000      | .000      | .00    |
| AM1 150 (MH)                      | .000      | .000      | .000               | .000     | .000      | .000      | .00    |
| HM1 IMP (MV)                      | .000      |           | .000               | .000     | .000      | .003      | .00    |
| AMI FILL WOTE                     | .000      | .000      | .000               | .000     | .000      | .000      | .00    |
| ANT EFFICIENCY                    | .000      | .000      |                    | . 000    | 000       |           |        |
| AMI EFFZANO EFF                   | .600      |           | .000               | .000     | .000      |           |        |
| WHEN BROKEN                       | BHCK ETCH |           | FIRING AL          | PRINTING | V/T PROBE | V/1 PROBE | DICING |
| CELL NAME                         | Dâ        | 09        | X1                 | ×10      | K7        | ×4        | ×5     |
|                                   |           |           |                    |          |           | 6.450     | 6.45   |
| AREH (CM2)                        | 6.450     | 6.450     | 6.450              | 6.450    | 6.450     | . 024     | .0.    |
| B.D. RHOLOHM-CM)                  | .028      | 1.511     | .000               | .000     | .000      | .000      | .00    |
| A.D.R-SOR(OHM)                    | .000      | 51.891    | 94.266             | 58.463   | 52.116    | 52.571    | 53.02  |
| AMO VOC (MV)                      | .000      | .000      | 586.000            | 582.000  | 222.000   | .000      | 218.00 |
| AMO 150 (MA)                      | .000      | .000      | 233.000<br>462.000 | 469.000  | 470.000   | .000      | 459.00 |
| AND VIP (MY)                      | .000      | .000      | 205.000            | 192.000  | 191.000   | .000      | 194.00 |
| AND FILL FOTE                     | .000      | .000      | .694               | .706     | .691      | .000      | .71    |
| AMO EFFICIENCY                    | .000      | .000      | .109               | .103     | .103      | .000      |        |
| AMI VOC CMV)                      | .000      | .000      | .000               | .000     | .000      | .000      | .01    |
| AM! ISC (MA)                      | .000      | .000      | .000               | .000     | .000      | .000      | . 0    |
| HILL THE CHY                      |           | .000      | .000               | .000     | .000      | .000      | .0     |
| HM1 FILL FOTR                     | .000      | .000      | .000               | .000     | .000      | .000      | .01    |
| AMI EFFICIENCY                    | .000      | .000      | .000               | .000     | .000      |           |        |
|                                   | .000      |           |                    |          |           |           |        |

#### Table 7 continued

|                  |         | EF        | .02     |           |  |
|------------------|---------|-----------|---------|-----------|--|
| CELL NAME        | N6      | ,×7       | ×s .    |           |  |
| HREA (CM2)       | 6.450   | 6.450     | 6.450   | 6.450     |  |
| THICK (CM)       | .043    | .022      | .022    | . 022     |  |
| B.D. RHOCOHM-CM) | .000    | .000      | .000    | 13.307    |  |
| A.D.R-SOR(OHM)   | 53.024  | 46.906    | 57.556  | 56.010    |  |
| AMO VOC (MV)     | 587.000 | 567.000   | 569.000 | .000      |  |
| AMO ISC (MA)     | 228.000 | 230.000   | 222.000 | .000      |  |
| AND VHP (NV)     | 474.000 | 470.000   | 473.000 | .600      |  |
| AMO IMP (MA)     | 197.000 | 202.000   | 197.000 | .000      |  |
| AMO FILL FCTR    | .698    | .703      | .713    | .000      |  |
| AND EFFICIENCY   | .107    | .109      | .107    | .000      |  |
| AMI VOC (MV)     | .000    | .000      | 000     | .000      |  |
| AMI ISC (MA)     | .000    | .000      | .000    | .000      |  |
| AMI VMP (MV)     | .000    | .000      | .000    | .000      |  |
| AMI IMP (MM)     | .000    | .000      | .000    | .000      |  |
| AM1 FILL FCTR    | .000    | .000      | .000    | .000      |  |
| AMI EFFICIENCY   | .000    | .000      | .000    | .000      |  |
| HM1 EFFZAMO EFF  | .000    | .000      | .000    | . 000     |  |
| WHEN BROKEN      |         | SIMULATOR |         | BACK ETCH |  |

Table 8

SPECTPAL SENSITIVITY

EFG02 64 C9 CELL NAME 65 67 C9 002 66 W.L. (MICRON) .211 .320 .328 .000 .000 .000 .000 7000 45 .000 .000 .000 .264 .000 .000 000 000 .000 .000 55 000 000 600 .303 .000 60 .000 .000 .000 .000 .263 65 262 .000 .000 600 .000 .000 .000 .000 .000 .000 .000 .000 .000 75 .000 .000 .000 .302 .220 .263 .220 .293 .154 000 000 .000 .204 000 .000 .000 .166 90 .000 .000 .000 .000 .000 .142 .000 .000 000 .000 .000 .090 1.05 . unu .000 .000 000 000 . 031 0.1 CELL NAME 02 0.3 05 07 04 Dé W.L. (MICPON) .000 .127 . 000 .000 . 000 .000 600 .264 .000 000 .000 .000 .000 .000 .000 . 000 . 000 ..000 55 050 .304 .000 .000 .000 .000 60 .000 .268 .000 .000 .000 .000 .000 262 65 .600 .000 . 000 .000 .000 .000 .000 .000 . 000 .000 .000 .000 75 .000 .006 .000 .000 .000 .000 20 000 204 .000 .000 .000 .000 .000 65 000 .000 0.10 000 .000. .000 90 .142 .000 . 000 . 000 .000 .000 .000 . 000 .000 .000 .000 --.000 -.000 1.05 .000 . 000 . 031 .000

Table 8 continued

|   |  |  | FC02   |   |  |   |   |
|---|--|--|--|---|--|---|---|
|   |  |  |  |   |  |   |   |
| A   |  | D9   | ×1   | . ×10   | х3   | ×4  | ×5  |
| W.L. (MICRON)   | - Cô   | 09   |  | ***************************************   |  |   |   |
|   |  |  |  |   |  |   |   |
| .41   | .000   | .000   | .129   | .129  | .262   | .000  | .201  |
| .50   | .000   | .000   | .172   | ,346  | .343   | .000  | .345  |
| 55  | .000   | .000   | .194   | .405  | .400   | .000  | .413  |
| .65   | .000   | .000   | .207   | .453  | .423   | .000  | .467  |
| 70  | .060   | .000   | .240   | .494  | .427   | .000  | .500  |
| .75   | .000   | .000   | .257   | .530  | . 534  | .000  | .543  |
| .80   | .000   | .0.6   | 276  | .554  | . 573  | .000  | :592  |
| .85   | .000   | .000   | .313   | .679  | .658   | .000  | .673  |
| .95   | .000   | .000   | .336   | .716  | .707   | .000  | .713  |
| 1.05  | .000   | .000   | .166   | .353  | .361   |   | .347  |
|   |  |  |  |   | **********   |   |   |
|   |  |  |  |   |  |   |   |
| CELL NAME   | 16   | X7   | X6   | 119   |  |   |   |
| W.L. (MICRON)   |  |  |  |   | //   |   |   |
|   |  |  |  |   |  |   |   |
| .45   | 377  | 161  | 247  | .060  |  |   |   |
|   | 515  |  | . 343  | .000  |  |   |   |
| .55   | 440  | 274  | 210  | .000  |  |   |   |
| .65   | .471   | 232  | .461   | .600  |  |   |   |
| .70   | .5 .6  | .317   | .495   | .3.6  |  |   |   |
| 75  | .547   | .340   | .532   | .300  |  |   |   |
| .80   |  | .346   | .595   | .000  | constitution a some manipul  |   |   |
| .90   | .663   | .464   | .644   | .000  |  |   |   |
| . 45  | .739   | 445  | .696   | .000  |  |   |   |
| 1.05  | .14*   | .252   | .370   | 000   |  |   |   |
|   |  |  |  |   |  |   |   |
|   |  | Tab  | ole 9  |   |  |   |   |
|   | RESISTIVITY  | AND ILLUM  | NATED CHAR   | ACTERISTICS   |  |   |   |
| *****   |  | HE   | M02  |   |  |   |   |
|   |  |  |  |   |  |   |   |
| CELL NAME   |  | - 10 -   | 11   | 12 -  | 13   | 14  | 15  |
|   |  |  |  |   |  |   |   |
|   | 4.000  | 4.000  | 4.000  | 4.000   |  | 4.000   | 4.000   |
| AREA (CM2)  |  | . 045  | .045   | . 045   | . 045  | .046  | . 046   |
| THICK (CH)  | . 045  |  | . 082  | 54.384  | 58.916   | 54.384  | -58.916   |
| HICK (CM)<br>B.D.RHO(OHM-CM)  | .000   | 61.635   | 58.916   |   |  |   |   |
| THICK (CH) B.D.RHO(OHM-CM) A.D.R-SOR(OHM) AMO VOC (MV)  | .000   | 61.635<br>587.000  | 567.000  | 567.000   | 585.000  | 597.000   | 594.000   |
| THICK (CM)  B.D.RHO(OHM-CM)  A.D.R-SOR(OHM)  AMO VOC (MV)  AMO ISC (M4)   | .000   | 61.635<br>587.000<br>131.000   | 122.000  | 125.000   | 130.000  | 135.000   | 131.000   |
| THICK (CM) B.D.RHO(OHM-CM) A.D.R-SOR(OHM) AMO VOC (MV) AMO ISC (M4) AMO VMP (MV)  | .000   | 61.635<br>587.000<br>131.000<br>472.000  | 567.000<br>122.000<br>482.000  | 567.000<br>125.000<br>- 493.000   | 130.000<br>480.000   | 597.000<br>135.000<br>495.000   | 131.000<br>483.000  |
| THICK (CH)  B.D.RHO(OHM-CM)  A.D.R-SOR(OHM)  AND VOC (MV)  AND ISC (NA)  AND VHP (MV)  AND IMP (NA)   | .000   | 61.635<br>587.000<br>131.000<br>472.000<br>119.000                                       | 567.000<br>122.000<br>482.000<br>106.000                                 | 567.000<br>125.000<br>493.000<br>119.000  | 130.000<br>130.000<br>480.000<br>120.000                                       | 597.000<br>135.000<br>495.000<br>125.000  | 594.000<br>131.000<br>483.000   |
| THICK (CM) B.D.RHO(OHM-CM) A.D.R-SOR(OHM) AMO VOC (MV) AMO ISC (M4) AMO VMP (MV)  | .000   | 61.635<br>587.000<br>131.000<br>472.000<br>119.000                                       | 567.000<br>122.000<br>482.000  | 567.000<br>125.000<br>- 493.000   | 585.000<br>130.000<br>460.000<br>120.000                                       | 597.000<br>135.000<br>495.000   | 594.000<br>131.000<br>483.000<br>118.000  |
| THICK (CH) B.D.RHO(OHM-CM) A.D.R-SOR(OHM) AMO VOC (MV) AMO ISC (H4) AMO VMP (MV) AMO IMP (MV) AMO IMP (MA) AMO FILL FCTP AMO EFFICIENCY AMI VOC (MV)              | .000<br>.000<br>.000<br>.000<br>.000                 | 61.635<br>587.000<br>131.000<br>472.000<br>119.000<br>.730<br>.104                       | 567.000<br>122.000<br>462.000<br>106.000<br>.713<br>.094                 | 567.000<br>125.000<br>493.000<br>118.000<br>.793<br>                                      | 585.000<br>130.000<br>480.000<br>120.000<br>.757<br>.106<br>562.000            | 597.000<br>135.000<br>495.000<br>125.000<br>.768<br>.114<br>598.000                       | 594.000<br>131.000<br>483.000<br>118.000<br>-732<br>-105                                  |
| THICK (CH) B.D.RHO(OHM-CM) A.D.R-SOR(OHM) AMO VOC (MV) AMO ISC (M4) AMO VMP (MV) AMO IMP (MA) AMO FILL FCTP AMO EFFICIENCY AMI VOC (MV) AMI ISC (MA)              | .000<br>.000<br>.000<br>.000<br>.000<br>.000         | 61.635<br>587.000<br>131.000<br>472.000<br>119.000<br>.730<br>.104<br>588.000<br>116.000 | 567.000<br>122.000<br>462.000<br>106.000<br>.713<br>.094                 | 567.000<br>125.000<br>493.000<br>119.000<br>.793<br>107<br>588.000<br>107.000             | 585.000<br>130.000<br>480.000<br>120.000<br>.757<br>-106<br>582.000<br>109.000 | 597.000<br>135.000<br>495.000<br>125.000<br>.768<br>.114<br>598.000                       | 594.000<br>131.000<br>483.000<br>118.000<br>.732<br>                                      |
| THICK (CH) B.D.RHOCOHM-CM) A.D.R-SOR(OHM) AMO VOC (HV) AMO ISC (H4) AMO VMP (HV) AMO IMP (HV) AMO FILL FCTR AMO EFFICIENCY AMI VOC (HV) AMI VOC (HV) AMI VMP (HV) | .000<br>.000<br>.000<br>.000<br>.000<br>.000<br>.000 | 61.635<br>587.000<br>131.000<br>472.000<br>119.000<br>.730<br>.104<br>588.000<br>478.000 | 567.000<br>122.000<br>462.000<br>106.000<br>.713<br>.094<br>.600<br>.600 | 567.000<br>125.000<br>493.000<br>119.000<br>.793<br>.107<br>588.000<br>107.000<br>497.000 | 585.000<br>130.000<br>480.000<br>120.000<br>757<br>                            | 597.000<br>135.000<br>495.000<br>125.000<br>.768<br>.114<br>599.000<br>116.000<br>498.000 | 594.000<br>131.000<br>493.000<br>118.000<br>.732<br>.105<br>593.000<br>110.000<br>491.000 |
| THICK (CM) B.D.RHO(OHM-CM) A.D.R-SOR(OHM) AMO VOC (MV) AMO ISC (M4) AMO VMP (MV) AMO IMP (MA) AMO FILL FCTR AMO EFFICIENCY AMI VOC (MV) AMI ISC (MA)              | .000<br>.000<br>.000<br>.000<br>.000<br>.000         | 61.635<br>587.000<br>131.000<br>472.000<br>119.000<br>.730<br>.104<br>588.000<br>116.000 | 567.000<br>122.000<br>462.000<br>106.000<br>.713<br>.094                 | 567.000<br>125.000<br>493.000<br>119.000<br>.793<br>107<br>588.000<br>107.000             | 585.000<br>130.000<br>480.000<br>120.000<br>.757<br>-106<br>582.000<br>109.000 | 597.000<br>135.000<br>495.000<br>125.000<br>.768<br>.114<br>598.000                       | 594.000<br>131.000<br>483.000<br>118.000<br>.732<br>                                      |

WHEN BROKEN

BACK ETCH 0 0 0 0 0 0

## Table 9 continued

#### RESISTIVITY AND ILLUMINATED CHARACTERISTICS

| ****** |                              |           |             | MO2         |             |         |           |         |
|--------|------------------------------|-----------|-------------|-------------|-------------|---------|-----------|---------|
|        |                              |           |             |             |             |         |           |         |
|        |                              |           |             |             |             |         |           |         |
|        | CELL NAME                    |           | ,           |             | 5           |         | <b> 7</b> |         |
|        | APEA (CM2)                   |           |             |             |             |         |           |         |
|        | THICK (CM)                   | 4.000     | 4.000       | 4.000       | 4.000       | 4.000   | 4.000     | .046    |
|        | B.D.RHOCOHM-CM>              | .063      | .082        | .061        | .062        | . 061   | .062      | .093    |
|        | A.D.R-SOR(OHM)               |           | 61.635      | 60.729      | 58.916      |         |           | 59.010  |
|        | AMO VOC (MV)                 | 593.000   | .000        | 131.000     | .000        | .000    | 132.000   | 132.000 |
| ***    | AMO VMP (MV)                 | 475.000   | .600        | 471.000     | .000        | .000    | 486.600   | 477.000 |
|        | AND IMP (MA)                 | 116.000   | .000        | 106.000     | .000        | .000    | 119.000   | 96.000  |
| -      | AMO FILL FCTR                |           | .000        | .651        | .000        | .000    | .744      | .609    |
|        | AMI VOC (MV)                 | .000      | .000        | .000        | .000        | .000    | 589.000   | .000    |
|        | AMI ISC (MA)                 | .000      | .000        | .000        | .000        | .000    | 113.000   | .000    |
|        | AMI IMP (MV)                 | .600      | .000        | .600        | .000        | .000    | 100.000   | .000    |
|        | AMI FILL FOTE                | .000      | .000        | .000        | .000        | .000    | .738      | .000    |
|        | AMI EFFICIENCY               | .000      | .000        | .000        | .000        | .000    |           |         |
|        | ANT EFF/AMO EFF              | .000      | .000        | .000        | .000        | .000    | 1.149     | .000    |
|        | WHEN BROKEN                  | UNLOADING | P EDGE ETCH | P EDGE ETCH | P NO RECORD | ? 0     | 0         | 0       |
|        |                              |           |             |             |             |         |           |         |
|        |                              |           |             |             |             |         |           |         |
|        | CELL NAME                    | •         | ×1          | ×2          |             | ×4      | ×5        | ×6      |
|        | AREA (CM2)                   | 4.000     | 4.000       | 4.000       | 4.000       | - 4.000 | 4.000     | 4.000   |
|        | THICK (CH)                   | . 046     | . 623       | .023        | . 623       | .023    | . 023     | . 123   |
|        | B.D.RHO(OHM-CM)              | .083      | .000        | .000        | 53.931      | .000    | 54.637    | 50.758  |
|        | A.D.R-SGR(OHM)               | 525.000   | 563.000     | 57.103      | 566.000     | 604.000 | .000      | 604.000 |
|        | AMO ISC (MA)                 | 130 000   | 144.000     | 153.000     | 143.000     | 150.000 | .000      | 153.000 |
|        |                              |           | 476.000     | 482.000     | 441.000     | 487.000 | .000      | 134.000 |
|        | AMO FILL FOTE                | 120.000   | 133.000     | 134.000     | 118.600     | 129.000 | .000      | .712    |
|        | AND EFFICIENCY               | .106      | .117        | .119        |             | .116    | .000      | .122    |
|        | AM1 VOC (NV)                 | .000      | 586.000     | .000        | .000        | .000    | .000      | .000    |
|        | AMI ISC (MA)<br>Ani VMP (MV) | .000      | 124.000     | .000        | .000        | .000    | .000      | .000    |
|        | AMI IMP (MA)                 | .000      | 116.000     | .000        | .000        | .000    | .000      | .600    |
|        | AMI FILL FOTE                | .000      | .761        | .000        | .000        | .000    | .000      | .000    |
|        | AMI EFFICIENCY               | .000      | 1.212       | .000        | .000        | .000    | .000      | .000    |
|        | HIII EFFERNO EFF             |           |             |             |             |         |           |         |
|        | WHEN BROKEN                  | 0         | 0           | 0           | 0           | 0       | NOT STABL | E O     |
|        |                              |           |             |             |             |         |           |         |
|        | CELL NAME                    | x7        | xe          |             |             |         |           |         |
|        | CECE HAME                    | ^′        |             |             |             |         |           |         |
|        | AREA (CM2)                   | 4.000     | 4.000       |             |             |         |           |         |
|        | THICK (CH)                   | .000      | .023        |             |             |         |           |         |
|        | A.D. R-SOR(OHM)              | 48.946    | 49.852      |             |             |         |           |         |
|        | AMO VOC (MV)                 | 595.000   | 595.000     |             |             |         |           |         |
|        | AMC ISC (MA)                 | 146.000   | 150.000     |             |             |         |           |         |
|        | AMO VMF (MV)                 | 482.000   | 464.660     |             |             |         |           |         |
|        | AMO FILL FCTR                | 136.000   | 109.000     |             |             |         |           |         |
| -      | AMO EFFICIENCY               | 123       | 097         |             |             |         |           |         |
|        | AM1 VOC (MV)                 | 585.000   | .000        |             |             |         |           |         |
|        | AMI ISC (MA)                 | 123.000   | 000         |             |             |         |           |         |
|        | ANI IMP (NA)                 | 116.000   | .000        |             |             |         |           |         |
|        | AMI FILL FOTE                | .786      | .000        |             |             |         |           |         |
|        | AMI EFFICIENCY               | 1.154     | .000        |             |             |         |           |         |
|        |                              |           |             |             |             |         |           |         |
|        | WHEN BROKEN                  | C         | 0           |             |             |         |           |         |

Table 10

57:

594

.000

.578

.541

.209

. ..... x7 ----

. 60

. 65

.90

.95

1.05

CELL NAME

.465

.460

.460

.361

XE

SPECTRAL SENSITIVITY HEMO2 CELL NAME 10 - 11------ 12------ 13------ 14 15 U.L. (MICRON) .104 .261 .372 .416 .447 .116 .277 .384 .434 .446 .470 .495 .105 .261 .379 .431 .467 .450 .101 .256 .355 .391 .178 .099 .251 .367 .101 .50 .257 .371 .425 .451 .420 .495 .495 .547 .60 .409 .456 454 .466 .450 .413 492 .75 .504 . 535 .460 561 535 :523 .575 .468 .532 .488 .351 .465 .552 .612 .90 .463 .273 .428 .398 .506 .382 . 95 . 396 .205 .343 .309 .454 .316 1.05 . 147 .218 . 054 . 095 . 681 .139 . 093 CELL NAME 2 3 W.L. (MICRON) .166 .41 .129 .128 .169 .139 .134 .168 .284 .394 .447 .500 .50 .293 .314 .289 .290 .321 .363 .397 .434 426 .424 . 433 .443 .478 .466 .424 .65 466 .453 .521 .451 .461 .491 .537 .480 .463 .496 .485 .526

| CELL   | Name     |      | ×-   | vo   |      |      | ×5     | ×6    |
|--------|----------|------|------|------|------|------|--------|-------|
|        |          |      |      |      |      |      |        |       |
| W.L. 6 | (MICRON) |      |      |      |      |      |        |       |
|        |          |      |      |      |      | MI   | 411.00 | M14 * |
|        | .41      | .119 | .116 | .120 | .115 | .146 | .000   | .138  |
|        | .45      | .275 | .274 | .276 | .273 | .289 | .000   | .263  |
|        | .50      | .396 | .396 | .394 | .390 | .395 | .000   | .392  |
|        | .55      | .440 | .456 | .448 | .453 | .459 | .000   | .461  |
|        | .60      | .479 | .494 | .477 | .486 | .501 | .000   | .503  |
|        | .65      | .497 | .512 | .514 | .513 | .522 | .000   | .529  |
|        | .70      | .522 | .545 | .543 | .548 | .566 | .000   | .564  |
|        | .75      | .558 | .591 | .587 | .594 | .620 | .000   | .621  |
|        | .80      | .591 | .625 | .611 | .622 | .656 | .000   | .652  |
|        | . 85     | .602 | .647 | .640 | .643 | .665 | .000   | .701  |
|        | .90      | .605 | .678 | .677 | .681 | .772 | .000   | .792  |
|        | .95      | .597 | .642 | .687 | .624 | .811 | .000   | .618  |
|        | 1.05     | .243 | .258 | .293 | .232 | .405 | .000   | .410  |

.495

.458

.424

.330

.502

512

.480

.493

.403

.169

493

50€

.465 .466

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.514

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564

.544

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.179

| U.L. (F                                |       | _     |       |  |
|--|-------|-------|-------|--|
|  |       |       |       |  |
|  | . • 1 | .120  | .176  |  |
|  | .45   | .279  | .314  |  |
| 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | .50   | .398  | .400  |  |
|  | .55   | .453  | .467  |  |
|  | .60   | .496  | .467  |  |
|  | .65   | .517  | .525  |  |
|  | .70   | .550  | .594  |  |
|  | .75   | . 554 | .678  |  |
| -                                      | .80   | .632  | . 651 |  |
|  | . 65  | .649  | .699  |  |
|  | .90   | .679  | .613  |  |
|  | .95   | .646  | .624  |  |
| 1                                      | . 05  | .259  | .405  |  |
|  |       |       |       |  |

Table 11

#### RESISTIVITY AND ILLUMINATED CHARACTERISTICS

|                | 00111 1 10000 ET 11181 1000 0gs 1 0                 |                   |         | ch03-1  |           |         |           |                    |
|----------------|---|-------------------|---------|---------|-----------|---------|-----------|--------------------|
|                |   |                   |         |         |           | ******* |           |                    |
|                | CELL NAME   | A1                | A2      | АЗ      |           | •• •    | 02        | 63                 |
|                | AREA (CM2)  | 4.000             | 4.000   | 4.000   | 4.000     | 4.000   | 4.000     | 4.000              |
|                | THICK (CM)  | .044              | .044    | . 045   | .044      | .044    | .046      | .044               |
|                | B.D.RHO(OHM-CM)                                     | .060              | .060    | . 061   | .061      | .081    | . 083     | . 081              |
|                | A.D.R-SOR(OHM)                                      | 42.601<br>591.000 | 598.000 | 606.000 | 40.335    | 550.000 | 43.507    | 41.694             |
|                | AMO ISC (MA)  | 118.000           | 128.000 | 137.000 | .000      | 123.000 | 130 000   | 598.000<br>134.000 |
| M. P. S. L. S. | AND VHP (MV)  | 466.000           | 561.000 | 507.000 | .000      | 484.000 | 249.000   | 478.000            |
|                | AMO IMP (MA)  | 96.000            | 121.000 | 129.000 | .000      | 117.000 | 108.000   | 125.000            |
|                | AMO FILL FCTR                                       | .653              | .792    | .766    | .000      | .794    | .446      | .746               |
|                | AND EFFICIENCY                                      | . 023             | .112    | .121    | .000      | .105    | . 049     | .110               |
|                | AMI VOC (MV)  | .000              | .000    | 121.000 | .000      | .000    | .000      | .000               |
|                | AMI VMP (MV)  | .000              | 000     | 509.000 |           | :000    | .000      | .000               |
|                | AMI IMP (MA)  | .000              | .000    | 113.000 | .000      | .000    | .000      | .000               |
|                | AMI FILL FCTR                                       | .000              | .000    | .766    | .000      | .000    | .000      | .000               |
|                | AMI EFFICIENCY                                      | .000              | .000    | .144    | .000      | .000    | .000      | .000               |
|                | AM1 EFF/AMO EFF                                     | .000              | .000    | 1.190   | .000      | .000    | .000      | .000               |
|                | UHEN BROKEN   | 0                 | 0       | 0       | SCRIBING  | 0       | 0         | 0                  |
|                |   |                   |         |         |           |         |           |                    |
|                | CELL NAME   | B4                | cı      | cs      | сз        | c4      |           |                    |
| -              | HREA (CH2)  |                   | 4.000   |         | 4.000     | 4.000   |           | 4.000              |
|                | THICK (CM)  | .046              | . 043   | .043    | .044      | . 044   | . 043     | . 043              |
|                | B.D. PHO CHM-CM)                                    | 43.054            | 39.428  | . 059   | 40.789    | 41.694  | . 059     | .059               |
|                | AND VOC (NV)  | 593.000           | 595.000 | 286.000 | 600.000   | 593.000 | .000      | 600.000            |
|                |   | 131.000           | 133.000 | 132.000 | 131.000   | 124.000 | .000      | 133.000            |
| -              |   | 492.000           | 484.000 | 180.000 | 500.000   | 491.000 | 000       |                    |
|                | AND IMP (MA)  | 121.000           | 117.000 | 105.000 | 121.000   | 110.000 | .000      | 125.000            |
|                | AMO FILL FOTR                                       | .766              | .716    | .501    | .770      | .735    | .000      | .786               |
|                |   | .110              | .105    |         | .112      | .100    | .000      | .116               |
|                | Ant Voc (NV)  | 592.000           | ,000    | .000    | 599.000   | .000    | .000      | 598.000            |
|                | AMI ISC (MA)  | 114.000           | .000    | .000    | 114.000   | .000    | .000      | 116.000            |
|                | AUT THE CHO   | 105.000           | .000    | .000    | 104.000   | .000    | .000      | 167.000            |
|                | AMI IMP (MA)  | 770               | .000    | .000    | .763      | .000    | .000      | .774               |
|                | AMI FILL FOTE<br>AMI EFFICIENCY<br>AMI EFFICAMO EFF | .130              | .000    |         | 130       | 000     |           | - 134              |
|                | ANT EFF. AND EFF                                    | 1.161             | .000    | .000    | 1.165     | .000    | .000      | 1.150              |
|                | WHEN BROKEN   | 0                 | ٥       | 0       | 0         | 0       | BACK ETCH |                    |
|                |   |                   |         |         |           |         |           |                    |
|                | CELL NAME   | 03                | D4      | е,      | - E2      |         | E4        | ·····              |
| ***            | AREA (CM2)  | 4.000             | 4.000   | 4.000   | 4.000     | 4.000   | 4.000     | 4.000              |
|                | THICK (CH)  | . 046             | . 046   | .043    | . 044     | . 044   | . 043     | .043               |
|                | A.D.R-SQR(OHM)                                      | 41.694            | 46.226  | 51.665  | 49.399    | 50.758  | 48.039    | 48.039             |
|                | AND VGC (MV)  | 588.000           | 578.600 | 453.000 | 569.000   | 493.000 | 522.000   | .000               |
|                | AMO 150 (MA)  | 126.000           | 120.000 | 130.000 | 116.000   | 122.000 | 110.000   | .000               |
|                | AMO VMP (MV)  | 484.000           | 476.000 | 272.000 | 473.000 - | 310.000 | 387.000   |                    |
|                | AMO IMP (MA)  | 110.000           | 112.000 | 100.000 | 107.000   | 90.000  | 76.000    | .000               |
|                | AMO FILL FOTR                                       | .707              | .769    | .462    | .754      | .464    | .526      | .000               |
|                | AND EFFICIENCY                                      | . 096             | . 099   | .050    | . 094     | . 052   | . 056     | .000               |
|                | AMI VOC (MV)  | .000              | .000    | .000    | 567.000   | .000    | .000      | .000               |
|                | AMI ISC (MA)  | .000              | .000    | .000    | 104.000   | .000    | .000      | :000               |
|                | AMI IMP (MV)  | .000              | .000    | .000    | 94.000    | .000    | .000      | .000               |
|                | AMI FILL FCTR                                       | .000              | .000    | .000    | .73e      | .000    | .000      | .000               |
|                | AMI EFFICIENCY                                      | .000              | .000    | .000    | .109      | .000    | .000      |                    |
|                | AMI EFF/AMO EFF                                     | .000              | .000    | .000    | 1.163     | .000    | .000      | ,000               |
|                | WHEN BROKEN   | DROPPED           | 0       | 0       | 0         | 0       | DROPPED   | SCRIBING           |

## Table 11 continued

#### RESISTIVITY AND ILLUMINATED CHARACTERISTICS

|      |                  |         | HE          | mo3-1        |           |                 |              |                      |
|------|------------------|---------|-------------|--------------|-----------|-----------------|--------------|----------------------|
|      |                  |         |             |              |           |                 |              |                      |
| ce   | LL NAME          | F2      | F3          | F4           | ×1        | ×2              | хз           | ×4                   |
|      | EA (CM2)         | 4.000   | 4.000       | 4.000        | 4.000 -   | 4.000           | 4.000        | 4.000                |
|      | ICK (CM)         | .043    | .000        | .000         | .023      | .023            | . 023        | . 023                |
|      | D. RHO( OHM-CM ) | .098    | .000        | .000         | .000      | .000            | .000         | .000                 |
|      | D.R-SGR(OHM)     | 47.359  | .000        | .000         | 577.000   | 46.660          | 593.000      | 581.000              |
|      | 10 ISC (MA)      | 114.000 | 124.000     | .000         | 139.000   | 140.000         | 139.000      | 131.000              |
| At   | 10 VMP (MV)      | 435.000 | 453.000     |              | - 466.000 | 482.600         | 476.000      | 493.060              |
|      | ( IMP (MA)       | 85.000  | 98.000      | .000         | 123.000   | 131.000         | 132.000      | 123.000              |
|      | O FILL FOTR      | .584    | .630        | .000         | .715      | .776            | .779         | .781                 |
|      | 11 VOC (MV)      | .000    | 567.000     | .000         | .000      | 581.400         | .000         | .000                 |
| At   | I ISC (MA)       | .000    | 109.000     | .000         | .000      | 121.000         | .000         | .000                 |
|      | I VMP (NV)       | .000    | 447.000     | .000         | 000       | 485.000         |              | .000                 |
|      | I IMP (MA)       | .000    | 85.000      | .000         | .000      | .766            | .000         | .000                 |
|      | FFECTENCY        | .000    | .615        |              | .000      | :135            | .000         |                      |
|      | I EFF/AMO EFF    |         | 1.158       | .000         | .000      | 1.154           | .000         | .000                 |
| U+   | EN BROKEN        | c       | 0           | SCRIBING     | ٥         | •               | DROPPED      | 0                    |
|      |                  |         |             |              |           |                 |              |                      |
| CE   | LL NAME          | ×5      | ×6          | X7           | ×e        |                 |              |                      |
| - 65 | E# (CH2)         | 4.000   | 4.000       | 4.000        | 4.000     |                 |              | ****                 |
| TH   | ICK (CH)         | . 0.27  | .023        | .023         | .023      |                 |              |                      |
|      | D. RHOK OHM-CM > | .000    | .600        | .000         | .000      |                 |              |                      |
|      | D.R-SORCOHM)     |         | 582.000     | 584.000      | 537.000   |                 |              |                      |
|      | 0 ISC (MA)       | 139.000 | 140.000     |              | 137.000   |                 |              |                      |
| 411  | O VMP KMV3       | 472.600 | 493.000     | 485.000      | 366.000   | W               |              |                      |
|      | O IMP (Mm)       | 132.000 | 132.000     | 131.000      | 71.000    |                 |              |                      |
|      | O FILL FOTE      | .769    | .782        | .786         | . 357     |                 |              |                      |
|      | 1 VOC (MV)       | .000    | 582.006     | 584.000      | .000      |                 |              |                      |
| A11  | 1 ISC (MA)       | .000    | 122.000     | 119.000      | .000      |                 |              |                      |
|      | I VMP (MV)       | .000    | 465.000     | 469.000      | .000      |                 |              |                      |
|      | I IMP (MH)       | .000    | 113.000     | 112.000      | .000      |                 |              |                      |
| 411  | EFFICIENCY       |         | 137         | .137         | .000      |                 |              |                      |
|      | I EFFZANO EFF    | .000    | 1.163       | 1.166        | .000      |                 |              |                      |
| UH   | EN BROKEN        | 0       | 0           | 0            | 0         |                 | ****         |                      |
|      |                  |         | Table       | e 12         |           |                 |              |                      |
|      |                  |         | SPECTRAL SE | NSITIVITY    |           |                 |              |                      |
|      |                  |         |             | 03-1         |           |                 |              |                      |
|      |                  |         |             |              |           | da 1.1.2.4      |              |                      |
| CEL  | NAME             | A,      | - A2        | са           | A4        | - 01            | 62 ····      | 63                   |
| W.L  | (MICRON)         |         |             |              |           |                 |              |                      |
|      | .41              | .106    | .117        | .135         | .000      | .134            | .135         | .135                 |
|      | .45              | .260    | .274        | .304         | .000      | .306            | .305         | .309                 |
|      | .50              | .364    | .322        | .415         | .000      | .407            | .420         | .458                 |
|      | .60              | .440    | .432        | 495          | .000      | .471            | .502         | .496                 |
|      | .65              | .457    | .484        | .514         | 000       | .471            | .512         | .511                 |
|      | .70              | .456    | .493        | .524         | .600      | .459            | .520         | .520                 |
|      |                  | .479    | .529        | .567         | .000      | 466             | .546         | .554                 |
|      | .65              | .463    | .559        | .571         | .000      | .429            | .541         | .594                 |
|      |                  |         |             |              |           |                 |              |                      |
|      | .90              | .434    | .541        | .588         | .000      | .355            | .492         | .570                 |
|      | .90<br>.95       | .301    | 487         | .552<br>.200 | .000      | - 1272<br>- 072 | .402<br>.125 | .570<br>.513<br>.189 |

## Table 12 continued

#### SPECTRAL SENSITIVITY

| ****          |      | не    | M03-1 |       |      | ***** |      |
|---------------|------|-------|-------|-------|------|-------|------|
|               |      |       |       |       |      |       |      |
| CELL NAME     |      | cı    | c2    | c3    | C4   | D1    | D2   |
| U.L. (HICROH) |      |       |       |       |      |       |      |
| .41           | .127 | .142  | .126  | .121  | .136 | .600  | .140 |
| .45           | .306 |       | .297  | .266  | .313 | .000  | .312 |
| .55           | .462 | .456  | .436  | .423  | .438 | .000  | .467 |
| .60           | .494 | .483  | .467  | .450  | .462 | .000  | .500 |
| .65           | .508 | .498  | .476  | .459  | .452 | .000  | .517 |
| .75           | .541 | .519  | .463  | .463  | .461 | .000  | .563 |
| .60           | .563 | .567  | .522  | .515  | .491 | .000  | .600 |
| .65           | .548 | .538  | .506  | .497  | .463 | .000  | .587 |
| .95           | .416 | 424   | .396  | 391   | .323 | .000  | .481 |
| 1.05          | .125 | .131  | .127  | .121  | .092 | .000  | .163 |
| ***           |      |       |       |       |      | ****  |      |
| CELL NAME     | D3   | D4    | c1    | E2    | E3   |       | F1   |
| W.L. (MICRON) |      |       |       |       |      |       |      |
| .41           | .000 | .133  | .113  | .111  | 100  | 000   | 000  |
| .45           | .000 | .306  | .260  | .276  | .102 | .000  | .000 |
| .50           | .000 | .404  | .408  | .365  | 368  | .000  | .000 |
| .55           | .000 | .459  | .454  | .423  | .434 | .000  | .630 |
| .65           | .000 | 444   | .499  | . 247 | .465 | .000  | .000 |
| .70           | .000 | .426  | .469  | .441  | .465 | .000  | .000 |
|               | .000 | .427  | .505  | .452  | .470 | .000  | .000 |
| . 65          | .640 | .374  | .480  | .406  | .433 | .000  | .000 |
| .90           | .000 | .303  | .395  | .327  | .351 | .000  | .000 |
| 1.05          | .000 | . 236 | . 309 | .062  | .269 | .000  | .000 |
|               |      |       |       |       |      |       |      |
| CELL NAME     | F2   | - F3  | F4    | X1    | ×5   | ×3    | ×4   |
| W.L. (MICRON) |      |       |       |       |      |       |      |
| .41           | .099 | .107  | .000  | .129  | .134 | .600  | .123 |
| .45           | .249 | .266  | .000  | .291  | .297 | .000  | .285 |
| .50           | .362 | .366  | .000  | .416  | .421 | .000  | .444 |
| .60           | .453 | .490  | .000  | .515  | .518 | .000  | .478 |
| .65           | .472 | .506  | .000  | .540  | .543 | .000  | .500 |
| .70           | .484 | .532  | .000  | .616  | .616 | .000  | .511 |
| .96           | .539 | 606   |       | .651  | 663  | .000  | .566 |
| .65           | .525 | .586  | .000  | .667  | .676 | .000  | .596 |
|               | .499 | .600  | .000  | .649  | .655 | 000   | .581 |
| 1.05          | .143 | .180  | .000  | .257  | .266 | .000  | .161 |
|               |      |       |       |       |      |       |      |
| W.L. (MICRON) | ×5   | X6    | ж7    | ×e    |      |       |      |
|               |      |       |       |       |      |       |      |
| -41           | .139 | .135  | .132  | .253  |      |       |      |
| .45           | .309 | .300  |       | .396  |      |       |      |
| .55           | .473 | .474  | .467  | .491  |      |       |      |
| .60           | .504 | .511  | .491  | .516  |      |       |      |
| .65           | .530 | .536  | .524  | .535  |      |       |      |
| .75           | .590 | .608  | .595  | .646  |      |       |      |
| .60           | .638 | .651  | .615  | .665  |      |       |      |
| .85           | .640 | .662  | .639  | .667  |      |       |      |
| 95            | .592 | .636  | 611   | .650  |      |       |      |
| 1.05          | .229 | .258  | .232  | .302  |      |       |      |

Table 13

#### RESISTIVITY AND ILLUMINATED CHARACTERISTICS

|                    | * .     |                  |           |           |          |           |          |
|--------------------|---------|------------------|-----------|-----------|----------|-----------|----------|
|                    |         |                  |           |           |          |           |          |
| CELL NAME          | - 21    | 23               | 24        | 25        | 26       | 27        | 26       |
| AREA (CM2)         | 4.000   | 4.000            | 4.000     | 4.000     | 4.000    | 4.000     | 4.00     |
| THICK (CH)         | . 625   | .025             | . 625     | .025      | .025     | .025      | 02       |
| B.D. RHOCOHM-CH)   | .000    | .000             | .000      | . 660     | .000     | .000      | .00      |
| A.D.P-SOR(OHM)     | 49.852  | 49.399           | 596.000   | 49.852    | 49.652   | - 602.000 | 599:00   |
| AMO VOC (MV)       | 128.000 | 125.000          | 122.000   | 126.000   | .000     | 128.000   | 128.00   |
| AND VMP (MV)       | 509.000 | 516.000          | .000      | . 600     | .000     | 515.000   | 511.00   |
| ano Inp (Ma)       | 119.000 | 116.000          | .000      | .000      | .000     | 116.400   | 115.000  |
| AMO FILL FCTR      | .767    | .797             | .000      | .000      | .000     | .776      | .760     |
| AMO EFFICIENCY     | .112    | 111              | .000      | .000      | .000     |           | .109     |
| AMI VOC (MV)       | 596.000 | 599.000          | . 000     | .000      | .000     | 110.000   | 110.000  |
| AMI ISC (MA)       | 511.000 | 517.000          | .000      | .000      | .000     | 515.000   | 511.000  |
| AMI IMP (MA)       | 102.000 | 98.000           |           |           | .000     | 100.000   | 99.000   |
| AMI FILL FOTE      | .792    | .791             | .000      | .000      | .000     | .762      | .776     |
| FEFTALF.           |         | .127             | .000      | .000      | .000     | .129      | . 126    |
| AMI EFF/AMO EFF    | 1.164   | 1.145            |           |           | 000      | 1.162     | -1:16    |
| WHEN BROXEN        |         |                  | SHORTED   | SHORTED   | CHIPPED  | CHIPPED   |          |
| CELL NAME          | 41      | 43               | 45        | 46        | 47       | 91        | 92       |
|                    |         |                  |           |           |          |           |          |
| HREM (CM2)         | 4.000   | 4.000            | 4.000     | 4.000     | 4.000    | 4.000     | 4.000    |
| THICK (CM)         | .025    | .025             | . 025     | .025      | . 625    | .025      | . 02     |
| B.D.RHO(OHM-CM)    | 52.571  | 49.652           | 49.652    | 49.399    | 48.946   | 45.320    | 46.22    |
| AMO VOC (MV)       | 586.000 | 363.000          | - 601.000 | 601.000   | 585.000- | 581.000   | 591:00   |
| amo ISC (MA)       | 122.000 | 124.000          | 128.000   | 128.000   | 123.000  | 120.000   | 124.00   |
| AND VMP (MV)       | 492,000 | 489.000          | 509.000   | 509.000   | 469.000  | 486.000   | 497.00   |
| HMO IMP (MH)       | 113.000 | 109.000          | 120.000   | 120.000   | 111.000  | 107.000   | 110.00   |
| AND FILL FOTE      | .778    | .731             | .794      | .794      | .754     | .749      | .74      |
| AND EFFICIENCY     | 563.000 | -591.000-        | -599.000  |           | 562.000  | 576.000   | 586.00   |
| AMI ISC (MA)       | 106.000 | 107.660          | 110.000   | 107.000   | 108.000  | 104.000   | 107.00   |
| ANT VMP (MV)       | 497.000 | 487.000          | 509.000   | .000      | 489.000  | 469.000   | 498.00   |
| HMT IMP (MH)       | 99.000  | 93.000           | 103.000   | .000      | 96.000   | \$2.000   | 96.00    |
| AM1 FILL FCTP      | .796    | .729             | .796      | .000      | .747     | .748      | .70      |
| AMI EFFICIENCY     | 1.197   | 1.160            | 1.161     |           | 1.170    | 7.766     | 1.19     |
| WHEN EROKEN        |         | CHIPPED          |           | SHORTED   |          |           |          |
|                    |         |                  |           |           |          |           |          |
| CELL NAME          | 94      | 97               | - 90      | ×10       | X11      | ×12       | ×13      |
| HREA (CH2)         | 4.000   | 4.000            | 4.000     | 4.000     | 4.000    | 4.000     | 4.00     |
| THICK (CII)        | .025    | .025             | .025      | :025      | .025     | .025      | .00      |
| B. C. RHOLOHM-CM > | .000    | .000             | 46.226    | 44.867    | 45.773   | 46.226    | 45 32    |
| H. D. P-SOF. OHM   | 598.000 | 567.000          | 599.000   | 601.000   | 597.000  | 601.000   | - 598.00 |
| AMO VOC (MV)       | 130.000 | 112.000          | 130.000   | 136.000   | 137.000  | 135.000   | 132.00   |
| AND VMP (MV)       | 502.000 | 463.000          | 501.000   | 506.000   | 502.000  | 514.000   | 509.00   |
| AMO IMP (MA)       | 115.000 | A0.000           | 116.000   | 127.000   | 123.000  | 123.000   | 123 00   |
| AMO FILL FOTE      | .743    | .563             | .746      | .786      | .755     | .779      | .79      |
| AMO EFFICIENCY     | .107    | .068             | .107      | - 599.000 | 594.000  | - 598:000 | - 596.00 |
| AMI VOC (IIV)      | 596.000 | 45.000<br>81.000 | 112.000   | 117.000   | 118.000  | 116.000   | 114.00   |
| AMI ISC (MH)       | 497.000 | .000             | 501.000   | 506.000   | 504.000  | 512.000   | 509 00   |
| AMI IMP (MH)       | 97.000  |                  | 99:000    | 109.000   | 106.000  | 106.000   | 105.00   |
| AMI FILL FOTE      | .729    | .000             | .742      | .767      | .762     | .762      | .76      |
|                    | .121    | .000             | .124      | .136      | .134     | .136      | .13      |
| AMI EFFICIENCY     | 1.130   | .000             | 1.155     | 17161     | 1.171    | 1.161     | 1.15     |

SHORTED

WHEN BROKEN

Table 13 continued

| CELL NAME        | X14     | ×2      |         | X4      | ×5      | X7      | к9      |
|------------------|---------|---------|---------|---------|---------|---------|---------|
| MPEH (CM2)       | 4.000   | 4.000   | 4.000   | 4.000   | 4.000   | 4.000   | 4.000   |
| THICK (CM)       | .025    | .025    | .025    | . 025   | . 025   | .025    | . 025   |
| B.D. PHOCOHM-CM> | .000    | .000    | .000    | .000    | .000    | .000    |         |
| A.D.R-SORCOHMY   | 46.226  | 51.665  | 48.946  | 48.039  | 49.399  | 50.758  | 45.326  |
| MITO VOC (MV)    | 597.000 | 564.000 | 561.000 | 601.000 | 599:000 | 134.000 | 136.000 |
| AMO 160 (MA)     | 509.000 | 137.000 | 135.000 | 510.000 | 513.000 | 511.000 | 513.000 |
| AMO VMF (MV)     | 124.000 | 128.000 | 123.000 | 126.000 | 125.000 | 126.000 | 127.000 |
| AMO FILL FOTE    | .769    | .792    | .764    | .786    | .767    | .801    | .794    |
| AMO EFFICIENCY   | .117    | .117    | .111    | .119    | .116    | .119    | .120    |
| AMI VOC (MV)     | 595.000 | 592.000 | 578.000 | 599.000 | 596:000 | 597.000 | 601.000 |
| AMI ISC (MA)     | 115.000 | 1.8.000 | 116.000 | 116.000 | 116.000 | 115.000 | 116.000 |
| AMI VMP (MV)     | 507 600 | 493.000 | 4:7.000 | 512.000 | 512.000 | 512.000 | 512.000 |
| AMI IMP (MH)     | 100.000 | 111.000 | 1.6.000 | 100.000 | 167.000 | 167.000 | 109.000 |
| AMI FILL FOTR    | .765    | .797    | .770    | .796    | .792    | .798    | .001    |
| AMI EFFICIENCY   | .134    | .137    | .129    | .138    | .137    | .137    | .140    |
| MI EFFZAMO EFF   | 1.152   | 1.169   | 1.766   | 1.164   | 1.156   | 1.151   | 1.159   |

WHEN BROKEN

| . 1           |             | SPECTRAL SI | ENSITIVITY |       |      |      |      |
|---------------|-------------|-------------|------------|-------|------|------|------|
|               |             | HE          | 104        |       |      |      |      |
|               |             |             |            |       |      |      |      |
|               |             |             |            |       |      |      |      |
|               | *********** |             |            |       |      |      | -    |
| CELL NAME     | 21          | 23          | 24         | 25    | 26   | 27   | 28   |
| W.L. (MICRON) |             |             |            |       |      |      |      |
| .41           | .116        | .113        | :104       | 106 - | .131 | .106 | .105 |
| .45           | .259        | .262        | .260       | .257  | .271 | .265 | .252 |
| .50           | .375        | .374        | .372       | .300  | .350 | .370 | .359 |
| .55           | .430        | .411        | .424       | .407  | .375 | :426 | .409 |
| .60           | .449        | .450        | .444       | .431  | .369 | .450 | .446 |
| .65           | .477        | .475        | .472       | .453  | .375 | .473 | .470 |
| .70           | .487        | .476        | .472       | .459  | .366 | .485 | .476 |
| .75           | .541        | .524        | .506       | .498  | .356 | .527 | .514 |
| .00           | .553        | .548        | .502       | .507  | .317 | .542 | .537 |
| .65           | .553        | .534        | .493       | .487  | .252 | .553 | .540 |
| .90           | .567        | .504        | .435       | .416  | .221 | .516 | .465 |
| .95           | .455        | .453        | .345       | .353  | .123 | .463 | .446 |
| 1.05          | .147        | .151        | .093       | .097  | .047 | .141 | .156 |

Table 14 continued

|               |       | LIE!  | MO4  |       |                        |       |       |
|---------------|-------|-------|------|-------|------------------------|-------|-------|
|               |       |       |      |       | *** ****** ** * * **** |       |       |
|               |       |       |      |       |                        |       |       |
|               |       |       |      |       |                        |       |       |
|               |       |       |      |       |                        |       |       |
| CELL NAME     | 41    | 43    | 45   | 46    | 47                     | 91    | 92    |
| W.L. (MICRON) |       |       |      |       |                        |       |       |
|               |       |       |      |       |                        |       |       |
| .41           | . use | . 092 | 360. | . 665 | . 697                  | . 691 | . 096 |
| .45           | .227  | .210  | .255 | .231  | .245                   | .218  | .240  |
| .50           | .341  | .344  | .354 | .344  | .362                   | .335  | .358  |
| .55           | . 394 | .400  | .405 | .365  | .409                   | .391  |       |
| .60           | .425  | .436  | .441 | .422  | .440                   | .430  | .436  |
| ,65           | .447  | .455  | .459 | .442  | .458                   | .466  | .457  |
| .70           | .470  | .474  | .460 | .465  | 1661                   | .474  | .445  |
| .75           | .505  | .512  | .510 | .500  | .521                   | .522  | .484  |
| .60           | .535  | .546  | .545 | .527  | .536                   | .544  | .496  |
| .65           | .522  | 540   | :544 | .532  | 539                    | .530  | :467  |
| .90           | .466  | .513  | .504 | .491  | .506                   | .498  | .377  |
| .95           | .432  | .453  | .459 | .436  | .454                   | .454  | .324  |

| CELL NAME      | 94   | 97   | 96   | XIO  | X11  | X12   | X13  |
|----------------|------|------|------|------|------|-------|------|
| W.L. (MICROIN) |      |      |      |      |      |       |      |
| .41            | .103 | .107 |      |      | .120 | .112  | .110 |
| .45            | .245 | .244 | .244 | .278 | .268 | .281  | .259 |
| .50            | .352 | .338 | .35€ | .415 | .404 | . 391 | .379 |
| .55            | .394 | .373 | .402 | .466 | .456 | .446  | :425 |
| .60            | .434 | .416 | .432 | .496 | .499 | .474  | .459 |
| .65            | .450 | .421 | .453 | .523 | .517 | .500  | .494 |
| .70            | .456 | .413 | .452 | .539 | .550 | .516  | .507 |
| .75            | .475 | .433 | .477 | .585 | .567 | .558  | .561 |
| .80            | .509 | .444 | .513 | .545 | .627 | .608  | .592 |
| .65            | .490 | .412 | .506 | .601 | .629 | .614  | .597 |
| .90            | .406 | .326 | .419 | .545 | .623 | .598  | .586 |
| .95            | .389 | .264 | .394 | .507 | .596 | .568  | .576 |
| 1.05           | .116 | .077 | .114 | .164 | .237 | .226  | .222 |

| CELL HERE     | X14  | ж2   |       | X4   | ×5   | 87   | х9   |
|---------------|------|------|-------|------|------|------|------|
| W.L. (MICRON) |      |      |       |      |      |      |      |
| -41           | .104 | .122 | .117  | .121 | .122 | .121 | .055 |
| .45           | .275 | .287 | .276  | .264 | .261 | .279 | .251 |
| .50           | .366 | .411 | .402  | .399 | .369 | .410 | .372 |
| .55           | .426 | .462 | .461  | .445 | .467 | .453 | .433 |
| .60           | .460 | .494 | .465  | .470 | .492 | .474 | .470 |
| .65           | .472 | .519 | .522  | .504 | .527 | .498 | .522 |
| .70           | .501 | .525 | .54e  | .516 | .536 | .518 | .522 |
| .75           | .559 | .586 | .602  | .574 | .580 | .574 | .554 |
| . 80          | .594 | .634 | .640  | .626 | .621 | .605 | .582 |
| .85           | .596 | .635 | . 635 | .629 | .628 | .622 | 559  |
| .90           | .580 | .624 | .627  | .635 | .616 | .604 | .494 |
| .95           | .543 | .604 | .593  | .611 | .571 | .574 | .451 |
| 1.65          | .196 | .241 | .226  | .239 | .211 | .220 | .137 |

Table 15

|                   |                    | Hel     | 106-1             |         |            |                 |         |
|-------------------|--------------------|---------|-------------------|---------|------------|-----------------|---------|
|                   |                    |         |                   |         |            |                 |         |
| CELL NAME         | A1                 | A10     | A11               | A12     | A13        | . A2            | A3 _    |
| AREA (CM2)        | 4.000              | 4.000   | 4.000             | 4.000   | 4.000      | 4.000           | 4.000   |
| THICK (CM)        | . 661              | .061    | 130.              | .061    | .061       | .061            | .061    |
| B.D. FHO (OHM-CM) | 3.329              | 3.329   | 3.329             | 2.329   | 47.133     | 45.773          | 3.329   |
| A.D.P.SOR(OHM)    | 45.320             | 51.665  | 48.946<br>575.000 | 577.000 | .000       | 578.000         | 582:000 |
| AMO VOC (MV)      | 138.000            | 139.000 | 136.000           | 140.000 | .000       | 138.000         | 141.000 |
| AMO UMP (MV)      | 491.000            | 460.000 | 476.000           | 476.000 | .000       | 482.000         | 480.000 |
| AND IMP (MA)      | 130.000            | 130.000 | 116.000           | 126.000 | .000       | .792            | .790    |
| AMO FILL FOTE     | .796               | .740    | .102              | .742    | .000       | .117            | .120    |
| AMO EFFICIENCY    | 550.000            | 000 -   | .000              | 000     |            | 580:000         | 582.000 |
|                   | 124.000            | .000    | .000              | .000    | .000       | 125.000         | 127.000 |
| AMI VMP (MV)      | 491.000            | .000    | .000              | .000    | .000       | 484.000         | 120.000 |
| AMI IMP (MH)      | 116.000            | .000    | .000              | .000    | .000       | .763            | .766    |
| AMI FILL FOTR     | .792               | .000    | .000              | .000    | .000       | .143            | .145    |
| AMI EFF/AMO EFF   | 17.207             | .000    |                   | :000    |            | 1:224           | 1.213   |
|                   |                    |         |                   |         | SPEC RESP  |                 | -0      |
| UHEN BROKEN       | ٥                  | 0       | . 0               |         | SPEC. KESP | . 0             |         |
| CELL NAME         | H4                 | A5      | 46                | H?      | A8         |                 | 61      |
|                   |                    |         |                   |         |            |                 |         |
| AREA (CM2)        | 4.000              | 4.000   | 4.000             | 4.000   | 4.000      | 4.600           | 4.000   |
| THICK (CM)        | .061               | .061    | . 061             | . 661   | .061       | 7.720           | 3.343   |
| B.D. RHOCOHM-CM)  | 3.329              | 3.329   | 3.329             | 49.652  | 3.329      | 3.329           | 45.773  |
| H.D.R-SOR. OHM /  | 46.226             | 578.000 | 579.000           | 569.000 | 556.000    | 572.000         | 566.000 |
| HMO VOC (MV)      | .000               | 140.000 | 137.000           | 135.000 | 138.000    | 139.000         | 133.000 |
| AND VIP (MV)      | .000               | 412.000 | 477.000           | 460.000 | 435.000    | 467.000         | 460.000 |
| AMO IMP (MA)      | .000               | 122.000 | 129.000           | 108.000 | 100.000    | 116.000         | 106.000 |
| AMO FILL FOTE     | .000               | .621    | .776              | .647    | .080       | .100            | .090    |
| AMO EFFICIENCY    | .000               | .000    | 579.000           |         | .000       |                 |         |
| AMI ISC (NA)      | .000               | .000    | 123.000           | .000    | .000       | .000            | .000    |
| ANT VMP (MV)      | .000               | .000    | 479.000           | .000    | 000.       | .000            | .000    |
| AM! IMP (MA)      | .000               | .000    | 115.000           | .000    | .000       | .000            | .000    |
| AMI EFFICIENCY    | .000               | .000    | .138              | .000    | .000       | .000            | .000    |
| ANTEFFZANO EFF    | .000               | .000    | -1.211            |         |            | . 000           | .000    |
| WHEN BROKEN       | EDGE ETCH          | 0       | ~                 | 0       | 0          | -0              |         |
|                   |                    |         |                   |         |            | B3              | 64      |
| CELL HAME         | B10                | 611     | - B12             | B13     | 62         |                 |         |
| AREA (CH2)        | 4.000              | 4.000   | 4.000             | 4.000   | 4.000      | 4.000           | 4.000   |
| THICK COND        | .061               | :061    |                   | 150.    | .061       | .061            | . 061   |
| B.D. RHOL CHM-CH. | 3.315              | 3.343   | 3.343             | 3.329   | 3.343      | 3.343<br>47.586 | 3.343   |
| A.D.R-SORCOHM     | 50.758             | 47.133  | 47.133<br>581.000 | 47.586  | 574.000    | - 575.000°      | 581.000 |
| AMO VOC (MV)      | 551.000<br>137.000 | 134.000 | 137.000           | .000    | 140.000    | 138 000         | 138.000 |
| AMO YER (MH)      | 397.000            | 244.000 | 466.000           | .000    | 413.000    | 477.000         | 476.000 |
| HMO INF (MH)      | \$6.000            | 95.000  | 129.000           | .000    | 105.000    | 126.000         | .775    |
| AMO FILL FOTE     | .505               | .408    | .766              | .000    | . 540      | .111            | .115    |
| AMO EFFICIENCY    |                    | .043    | 581.000           |         |            |                 | 580.000 |
| ANT ISC CHAP      | .000               | .000    | 124.000           | .000    | .000       | .000            | 124.000 |
| AMI VMP (MY)      | .000               | .000    | 482.000           | .000    | .000       | .000            | 116.000 |
| HMT INP (MA)      | .000               | .000    | .776              | .000    | .000       | .000            | .773    |
| AMI FILL FOTE     | .000               | .000    | .140              | .600    | .000       | .000            | .139    |
| AMT EFF/HMO EFF   |                    |         | 1.207             |         | 000        | .000            | 1.210   |

Table 15 continued

|                  |         | · #A    | HCE-1    |         |          |         |         |
|------------------|---------|---------|----------|---------|----------|---------|---------|
| CELL NAME        | 65      | B6      |          | 66      |          | xı      | N2      |
|                  |         | 4.000   | 4.000    | 4.000   | 4.000    | 4.000   | 4.000   |
| AREA (CM2)       | 4.000   | .061    | .061     | 160     | .061     | .023    | . 023   |
| THICK (CM)       | 3.343   | 3.343   | 3.329    | 3.329   | 3.329    | .000    | .000    |
| B.D. RHOLOHM-CM) | 46.492  | 48.946  | 46.226   | 50.758  | 53.024   | 45.320  | 46.226  |
| A.D.R-SOR(OHM)   | 577.000 | 571.000 | -462.000 | 579:000 | 578.000  | 598:000 | 596.00C |
| AMO ISC (NA)     | 135.000 | 139.000 | 133.000  | 139.000 | 138.000  | 135.000 | 136.000 |
| AND VER (MV)     | 482.000 | 473.000 | 268.000  | 480.000 | 481.000  | 507.000 | 502.000 |
| AND IMP (MA)     | 126.000 | 118.000 | 95.000   | 130.000 | 131.000  | 129.000 | 716.000 |
| ANG FILL FOTR    | .780    | .703    | .414     | .775    | .790     | 810     | .716    |
| AMO EFFICIENCY   |         |         | .047     | .115    | ,116     | .121    | .108    |
| AMI VOC (NV)     | 576.000 | .103    | .000     | 578.000 | 576.000  | 595.060 | .000    |
| AMI ISC (MA)     | 121.000 | .000    | .000     | 125.000 | 124.000  | 120.000 | .000    |
| AMI VMP (NV)     | 430.000 | .000    | .000     | 479.000 | 486.000  | 502.000 | .000    |
| ANT IMP (MA)     | 113.100 | .000    | .000     | 116.000 | 115.000  | 114.000 | .000    |
| AMI FILL FOTR    | .778    | .000    | .000     | .769    | .763     | .802    | .000    |
| AMI EFFICIENCY   | .136    | .000    | .000     | .139    | .140     | .143    | .000    |
| HHI EFF AND EFF  | 1.208   | .000    | .000     | 7.205   | 1.205    | 1:164   | .000    |
| WHEN BROKEN      | -0      | - 0     |          | 0       | -0       |         |         |
| CELL NAME        | N3      | N4      | xs       | Хé      | ×7       | ×8      |         |
| AREA (CM2)       | 4.000   | 4.000   | 4.000    | 4.000   | 4.000    | 4.000   |         |
| THICK (CM)       |         |         |          | .023    | .023     | .023    |         |
| B.D. RHOCOHM-CM  | .000    | .000    | .000     | .000    | .000     | .000    |         |
| A.D.R-SOR(OHM)   | 49.852  | 50.758  | 48.492   | 47.586  | 47.506   | 50.758  |         |
| EMO VOC (MV)     | 594.000 | 558.000 | 553.000  | 556.000 | 563.000  | .000    |         |
| AND ISC (MH)     | 135.000 | 135.000 | 145.000  | 134.000 | 145.000  | .000    |         |
| AMO VIIP (MV)    | 501.000 | 564.000 | 484.000  | 304.000 | 492.000  | .000    |         |
| Amo Imp (mm)     | 127.000 | 125.000 | 137.000  | 127.000 | 137.000  | .000    |         |
| AMO FILL FOTR    | .793    | .760    | .764     | .801    | .761     | .000    |         |
| AND EFFICIENCY   | .118    | .116    | . 123    | .118    | 581:000- | :000    |         |
| ANT VOC (MV)     | .000    | .000    |          |         | 128.600  | .000    |         |
| ANT ISC (MA)     | .000    | .000    | .000     | .000    | 485.000  | .000    |         |
| AMI VMP (MV)     | .000    | .000    | .000     | .000    | 120.000  | -000    |         |
| ent Imp (ma)     | .000    | .000    | 7,000    | .000    | .763     | .000    |         |
| AMI FILL FOTE    | .000    | .000    | .000     | .000    | .146     | .000    |         |
| AMI EFFICIENCY   | ,000    | .000    | 000      |         | T. 192   |         |         |
| THMT EFFZAND EFF |         | :000    | .000     | .000    | 1.172    |         |         |

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Table 16
GARK CURPENT DENSITY, RUN HARCE-1

Table 16 continued

| Vp/5/N    | C1     | C3     | cı     | C.     | cs     | C6     | C7     | Vp/5/N    | Al     | A2     | A)     | AS     | A6     | A7     |
|-----------|--------|--------|--------|--------|--------|--------|--------|-----------|--------|--------|--------|--------|--------|--------|
| .01 Volts | 5.0-08 | 4.5-08 | 1.3-07 | 3.8-08 | 6.0-00 | 5.8-08 | 1.3-06 | .01 Volte | 2.7-07 | 2.0-08 | 7.5-09 | 1.3-08 | 4.8-08 | 1.7-06 |
| .04       | 2.2-07 | 2.6-07 | 6.0    | 2.2-07 | 2.8-07 | 2.7-07 | 5.0    | .04       | 1.1-06 | 0.0    | 4.0-00 | 4.5    | 2.7-07 | 2.2-05 |
| .00       | 5.6    | 1.4    | 1.6-06 | 1.5    | 0.2    | 7.7    | 1.5-07 | .01       | 2.3    | 2.1-07 | 1.3-07 | 1.7-07 | 7.3    | 7.9    |
| .10       | 1.2    | 1.2-06 | 2.5    | 1.5-06 | 1.3-06 | 1.2-06 | 2.3    | .10       | 3.0    | 3.0    | 2.1    | 2.6    | 1.2-06 | 1.2-04 |
| .15       | 1.4-06 | 2.9    | 6.6    | 4.0    | 3.0    | 3.4    | 61.    | .15       | 5.0    | 9.6    | 5.4    | 6.0    | 1.7    | 1.7    |
| .20       | 2.7    | 5.0    | 1.6-05 | 1.1-05 | 1.0    |        | 1.6-06 | .20       | 7.3    | 2.3-06 | 1.4-06 | 1.4-06 | 1.5    | 7.0    |
| .25       | 4.8    | 1.1-05 | 3.6    | 2.2    | 1.8-05 | 2.0-05 | 4.0    | .25       | 1.1-65 | 5.0    | 3.4    | 3.6    | 2.0-05 | 1.4-03 |
| . 30      | 1.5    | 1.9    | 7.3    | 3.0    | 3.3    | 3.0    | 9.0    | . 30      | 1.6    | 1.1-05 | 1.6    | 9.6    | 1.9    | 2.3    |
| . 25      | 1.5-05 | 3.5    | 1.4-04 | 6.2    | 6.1    | 7.0    | 2.4-05 | .35       | 2.7    | 2.8    | 2.4-05 | 2.5-05 | 0      | 1.4    |
| .40       | 2.5    | 1.0    | 2.5    | 1.1-04 | 1.2-04 | 1.3-04 | 6.6    | .40       | 4.4    | 7.4    | 6.6    | 7.7    | 1.6-04 | 4.7    |
| .45       | 3.9    | 1.9-04 | 5.1    | 2.3    | 3.0    | 2.9    | 2.4-04 | .45       | 2.3-04 | 2.5-04 | 2.3-04 | 2.8-04 | 4.2    | 6.3 .  |
| .50       | 5.1    | 7.6    | 1.3-03 | 7.2    | 7.2    | •.5    | •.0    | .50       | 1.1-03 | 1.3-03 | 1.1-03 | 1.1-03 | 1.3-03 | 9.0    |
| v,        |        |        |        |        |        |        |        | v,        |        |        |        |        |        |        |
| .05 Volts | 2.2-07 | 1.6-07 | 5.0-07 | 8.0-08 | 2.1-07 | 1.9-07 | 4.8-08 | .05 Volts | 1.2-06 | 4.5-08 | 3.0-08 | 6.5-08 | 1.2-07 | 8.2-06 |
| .10       | 4.4    | 2.5    | 1.4    | 1.2-07 | 3.5    | 3.0    | 1.3    | .10       | 2.5    | 7.0    | 4.1    | 1.1-07 | 1.9    | 1.2-05 |
| .20       | 1.1    | 4.0    | 1.9-06 | 1.6    | 5.8    | 4.4    | 1.5-07 | .20       | 5.7    | 1.1-07 | 0      | 1.8    | 2.9    | 1.4    |
| .30       | 1.4-06 | 5.6    | 2.9    | 1.9    | 7.9    | 5.6    | 2.2    | .30       | 1.4    | 1.6    | 1.1-07 | 2.5    | 3.7    | 1.7    |
| .40       | 2.0    | 1.3    | 4.2    | 2.3    | 1.1    | 6.7    | 2.9    | .40       | 1.4-05 | 2.2    | 1.4    | 3.3    | 4.6    | 2.0    |
| .50       | 2.6    | 1.1-06 | 5.6    | 2.6    | 1.2-06 | 7.7    | 3.7    | .50       | 1.9    | 2.7    | 1.6    | 3.9    | 5.3    | 2.3    |
| .60       | 3.2    | 1.3    | 7.4    | 3.0    | 1.4    | 1.4    | 4.4    | .60       | 2.5    | 3.4    | 1.9    | 4.6    | 6.3    | 2.7    |

#### Table 16 continued

|                     |        | Tel    | bie 16 co | teunia |        |        |            |                     |        |        |        |        |        |        |
|---------------------|--------|--------|-----------|--------|--------|--------|------------|---------------------|--------|--------|--------|--------|--------|--------|
| V <sub>P</sub> /5/3 |        | 9.2    | 63        | 9.2    | 85     | 26     | <b>B</b> 7 | V <sub>F</sub> /5/N | AE     | A9     | A10    | *41    | A12    | A13    |
| .01 Volts           | 5.2-06 | 4.5-68 | 6.0-07    | 5.5-08 | 1.2-08 | 1.8-06 | 1.1-05     | .01 Volts           | 1.2-05 | 2.0-06 | 1.5-08 | 2.5-06 | 6.3-07 | 5.5-04 |
| .04                 | 2.1-05 | 2.1-07 | 4.5-06    | 2.9-07 | 5.3    | 1.1-05 | 2.8        | .01                 | 6.6    | 1.0-05 | 4.3    | 1.4-05 | 3.9-06 | 2.7-03 |
| .06                 | 6.9    | 5.6    | 1.5-65    | 9.1    | 1.5-07 | 3.4    | 1.7-04     | .06                 | 2.0-04 | 3.9    | 1.1-07 | 4.4    | 1.3-05 | 7.4    |
| .10                 | 1.1-04 | 1.2-06 | 2.5       | 1.5-66 | 2.2    | 5.8    | 5.7        | .10                 | 3.2    | 6.1    | 1.4    | 7.7    | 2.2    | 1.1-02 |
| .15                 | 3.1    | 3.8    | 7.6       | 4.1    | 5.5    | 1.5-04 | 9.5        | .15                 | 1.2    | 1.8-04 | 3.6    | 2.2-04 | 6.4    | 2.1    |
| .20                 | 7.3    | 1.1-05 | 1.6-04    | 1.1-05 | 1.4-06 | 3.5    | 2.4-03     | .2:                 | 1.7-03 | 4.4    | 1.6    | 4.5    | 1.4-04 |        |
| .25                 | 103    | 2.6    | 3.1       | 2.4    | 3.5    | 6.4    | 4.1        | .25                 | 2.9    | 6.3    | 2.1-06 | 0.3    | 2.7    |        |
| . 30                | 2.4    | 5.1    | 5.2       | 4.6    | 9.2    | 1.1-03 | 1.2        | . 30                | 4.4    | 1.5-03 | 5.4    | 1.3-03 | 4.6    |        |
| . 35                | 3.5    | 1.0+04 | 1.1       | 6.9    | 2.5-05 | 1.6    | 1.2-02     | . 35                | 6.1    | 2.2    | 1.6-05 | 2.0    | 7.2    |        |
| .40                 | 5.0    | 1.8    | 1.3-03    | 1.7-04 | 7.5    | 2.3    | 1.7        | .40                 | 1.4    | 3.3    | 5.2    | 2.6    | 1.1-03 |        |
| .45                 | 6.9    | 3.3    | 1.9       | 3.8    | 2.9-04 | 3.4    | 2.3        | .45                 | 1.1-02 | 4.6    | 2.1-04 | 3.6    | 1.7    |        |
| .50                 | 5.6    | 1.1-03 | 2.4       | 1.3-00 | 1.3-03 | 5.4    |            | .50                 | 1.4    | 7.1    | 1.0-03 | 5.3    | 3.0    |        |
| v <sub>p</sub>      |        |        |           |        |        |        |            | v <sub>k</sub>      |        |        |        |        |        |        |
| .05 Volts           | 1.3-05 | 1.7-67 | 1.7-06    | 1.4-07 | 4.5-08 | 3.3-06 | 7.1-05     | .05 Volts           | 2.9-05 | 3.3-06 | 3.3-08 | 5.1-06 | 2.0-06 | 1.5-0  |
| .10                 | 2.2    | 1.8    | 2.1       | 3.1    | 7.8    | 5.2    | 9.8        | .10                 | 4.1    | 5.0    | 5.5    | 1.0-05 | 3.2    | 2.0    |
| .20                 | 4.6    | 2.6    | 4.5       | 4.5    | 1.3-07 | 7.7    | 1.4-04     | .20                 | 3.5    | 7.2    | 9.5    | 1.4    | 4.6    | 2.6    |
| . 10                | 6.9    | 3.8    | 5.9       | 5.7    | 1.7    | 9.9    | 1.7        | .30                 |        | 1.6    | 1.3-07 | 1.7    | 6.0    | 3.0    |
| .40                 | 9.7    | 4.7    | 7.3       | 615    | 2.0    | 1.0-05 | 1.9        | .40                 | 8.1    | 9.6    | 1.7    | 2.1    | 6.9    | 3.5    |
| .50                 | 1.3-04 | 6.0    | 1.7       | 7.3    | 2.3    | 1.1    | 2.0        | .50                 | 9.2    | 1.1-05 | 2.7    | 2.3    | 7.3    | 3.9    |
| .60                 | 1.6    | 6.7    | 1.0-05    | 1.3    | 1.7    | 1.1    | 2.2        | .60                 | 1.0-04 | 1.1    | 3.3    | 2.5    | 7.6    | 4.3    |

| V <sub>F</sub> /S/N | **     |        | <b>810</b> | 811    | 812    |
|---------------------|--------|--------|------------|--------|--------|
| .01 Volte           | 2.0-07 | 2.7-07 | 1.2-05     | 3.8-05 | 2.5-08 |
| .01                 | 9.8    | 1.1-06 | 6.6        | 2.1-04 | 1.1-07 |
| .01                 | 3.0-06 | 2.6    | 2.3-04     | 7.2    | 2.7    |
| .10                 | 4.0    | 4.1    | 3.7        | 1.7-03 | 4.1    |
| .15                 | 1.3-05 | 9.7    | 9.7        | 3.3    | 1.0-06 |
| .20                 | 3.2    | 2.2-05 | 2.0-03     | 4.6    | 2.6    |
| .25                 | 6.6    | 4.2    | 3.4        | 1.1-02 | 6.4    |
| . 30                | 1.2-04 | 7.4    | 5.1        |        | 1.5-05 |
| . 35                | 2.1    | 1.3-04 | 7.2        |        | 3.3    |
| .40                 | 3.5    | 2.4    | 9.5        |        | 0.2    |
| .45                 | 6.8    | 5.2    | 1.2-02     |        | 2.6-94 |
| .50                 | 1.6-03 | 1.6-03 | 1.6        |        | 1.4-03 |
| v <sub>R</sub>      |        |        |            |        |        |
| .05 Volts           | 6.4-07 | 1.2-06 | 2.9-05     | 8.3-05 | 1.3-07 |
| .10                 | 1.3-06 | 2.0    | 4.3        | 1.2-04 | 2.5    |
| .20                 | 2.8    | 4.2    | 6.3        | 1.6    | 5.3    |
| . 30                | 4.9    | 6.6    | 7.9        | 1.7    | 1.6    |
| .40                 | 7.5    | 9.4    | 8.1        | 1.9    | 1.2-06 |
| .52                 | 1.1-05 | 1.3-05 | 8.3        | 2.0    | 1.5    |
| .60                 | 1.4    | 1.6    | 8.6        | 2.1    | 1.9    |

Table 17

| SPECTARL SENSITIVITY  HANCE-1 |       |      |      |      |      |      |      |  |  |
|-------------------------------|-------|------|------|------|------|------|------|--|--|
| CELL NAME                     | н1    | A10  | A11  | A12  | H13  | A2   | H3   |  |  |
| W.L. (MICRON)                 |       |      |      |      |      |      |      |  |  |
|                               | .122  | .134 | .120 | .131 | .666 | .119 | .126 |  |  |
| .45                           | .271  | .290 | .264 | .289 | .000 | .272 | .294 |  |  |
| .50                           | .352  | .464 | .306 | .402 | .000 | .393 | .403 |  |  |
| .55                           | - 437 | .446 | .432 | .447 | .000 | .440 | .448 |  |  |
| .60                           | .483  | .512 | .499 | .512 | .000 | .510 | .515 |  |  |
| .65                           | .492  | .505 | .497 | .507 | .000 | .508 | .511 |  |  |
| .70                           | .523  | .531 | .525 | .536 | .000 | .534 | .539 |  |  |
| .75                           | .552  | .608 | .562 | .572 | .000 | .571 | .577 |  |  |
| .80                           | .827  | .692 | .670 | .685 | .000 | .665 | .890 |  |  |
| . 85                          | .624  | .633 | .625 | .634 | .000 | .635 | .642 |  |  |
| .90                           | .625  | .602 | .545 | .607 | .000 | .606 | .611 |  |  |
| .95                           | .565  | .592 | .579 | .587 | .000 | .564 | .605 |  |  |
| 1.05                          | .240  | .244 | .230 | .240 | .000 | .240 | .251 |  |  |

Table 17 continued

|               |             | на     | MCB-1      |      |       |       |       |
|---------------|-------------|--------|------------|------|-------|-------|-------|
|               |             |        |            |      |       |       |       |
| CELL NAME     | A4          | A5     | 46         | 47   | 40    | 49    | 81    |
| U.L. (MICRON) |             |        |            |      |       |       |       |
| -41           | .000        |        | :121       | .115 | .115  | .124  | .107  |
| .45           | .000        | .295   | .277       | .266 | .259  | .275  | .266  |
| .55           |             | .454   | : 396      |      |       |       | .383  |
| .60           | .000        | .516   | .512       | .508 | .466  | .512  | .503  |
| .65           | .000        | .512   | .505       | .501 | .510  | .506  | .507  |
| .75           | .000        | .575   | .579       | .565 | .508  | .576  | .535  |
| .80           | .000        | .862   | .669       | .670 | .634  | .662  | .633  |
| . 25          | .000        | .638   | .632       | .629 | .599  | .641  | .627  |
| .95           | .000        | .593   | .582       | .605 | .576  | .628  | .615  |
| 1.05          | .000        | .233   | .233       | .231 | .261  | .243  | :221  |
|               |             |        |            |      |       |       |       |
| CELL HAME     | 85          | 86     | _ 67       | 68   | 69    | X1    | x2    |
| W.L. (MICRON) |             |        |            |      |       |       |       |
| .41           | .122        | 7127   | .126       | .135 | .125  | .117  | .126  |
| .45           | .277        | .206   | .277       | .293 | .283  | .269  | .279  |
|               | 441         | .455   |            | .407 | .453  |       | .369  |
| .60           | .505        | .520   | .494       | .520 | .517  | .462  | .477  |
| .65           | .501        | 502    | .497       | .515 | .513  | .472  | .467  |
| .75           | .557        | .536   | .506       | .542 | .538  | .516  | .565  |
| .80           | . 653       | .877   | .851       | .878 | .878  | .782  | .762  |
| . 65          | .613        | .620   | .624       | .639 | .639  | .613  | .609  |
| .95           | .544        | .582   | .620       | .614 | .560  | .639  | .560  |
| 1.05          | .209        | . 233  | .235       | .229 | . 236 | .237  | .206  |
| CELL NAME     | <b>B</b> 10 | B11    | 613        |      | •     |       |       |
| W.L. (MICPON) | B10         | "!     | <u>612</u> | 613  | B2    | 63    | 84    |
|               |             |        |            |      |       |       |       |
| .41           | .122        | 124    | .119       | .126 | .132  | .128  | .128  |
| .50           | .401        | .394   | .273       | .282 | .289  | .402  | .235  |
| .55           | .453        | .453   | .452       | .453 | .455  | .447  | .448  |
| .60           | .519        | .506   | .509       | .515 | .519  | .516  | .509  |
| .70           | .543        | .536   | .542       | 540  | .541  | .534  | .536  |
| .75           | .579        | .571   | .560       | .575 | .575  | .566  | .531  |
| . 85          | 864         | 675    |            | 640  | 657   | .629  | 594 - |
| .90           | .635        | .622   | .635       | .624 | .615  | .661  | .576  |
| 1.05          | .595        | .576   | 251        | .593 | .573  | .565  | .569  |
| Y-1           | ×3          |        |            | X-6  | ¥7    | Xá    |       |
| V.L. (MICRON) | ×3          | X4     | ×5         |      |       |       |       |
| .41           | .126        | .121   | .125       | .120 | .125  | . 600 |       |
| .45           | .279        | .266   | .275       | .275 | .276  | .000  |       |
| .50           | .431        | 427    | .391       |      | 454 - | 000   |       |
| .60           | .476        | .470   | .501       | .481 | .474  | .000  |       |
| .65           | .485        | .492   | .534       | .494 | .532  | .000  |       |
| .70           | .511        | .463   | .565       | .521 | .569  | .000  |       |
| .80           | .785        | .800   | .646       | .747 | .864  | .000  |       |
| . 85          | .606        | .617   | .660       | .614 | .650  |       |       |
| .90           | .615        | .631   | .645       | .625 | .641  | .000  |       |
| 1.05          | .216        | - :230 | .258       | :221 | .252  | 000   |       |

Table 18

|                               |           | - Hester     | CG-2 .             |           |           |           |          |
|-------------------------------|-----------|--------------|--------------------|-----------|-----------|-----------|----------|
|                               |           |              |                    |           |           |           |          |
| CELL MANE                     | 161       | 162          | 171                | 112       | 211       | 212       | 371      |
| CELL MAIL                     |           |              |                    |           |           |           |          |
| AREA (CH2)                    | . 4.000   | 4.000        | 4.000              | 4.000     | -4:000 -  | 4.000     | 4.000    |
| THICK (CH)                    | . 661     | .061         | 3.272              | 3.272     | 2.172     | 2.172     | 2.135    |
| B.D.RHO(OHM-CM)               | 1.989     | 1.989        | 41.241             | .000      | .000      | .000      | 43.507   |
| A.D.R-SOR(OHN)                | 500.000   | .000         | .000               | .000      | .000      | .000      | 579.000  |
| AMO ISC (MA)                  | 135.000   | .000         | .000               | .000      | .000      | .000      | 479.000  |
| AMO VMP (MV)                  | 475.000   | 000          |                    | -000      | - 000     |           | 127.000  |
| AMO IMP (MA)<br>AMO FILL FOTR | 127.000   | .000         | .000               | .000      | .000      | .000      | .773     |
| AMO EFFICIENCY                | .111      | .000         | .000               | . 600     | .000      | .000      | 580 000  |
| ANT VOC (NV)                  | 590.000   | .000         | .000               | .000      | .000      | .000      | 120.000  |
| AMI ISC (MA)                  | 119.000   | .000         | .000               | .000      | .000      | .000      | 462.000  |
| ant Inp (NV)                  | 113.000   |              |                    | .000      |           |           | -111.000 |
| AMI FILL FOTE                 | .778      | .000         | .000               | .000      | .000      | .000      | .769     |
| ANT EFFICIENCY                | .134      | .000         | .000               | .000      |           | .000      | 1.190    |
| AM1 EFF/AMO EFF               | 1.204     | .000         | .000               | .000      | .000      |           |          |
| WHEN BROKEN                   | -0        | CHEM POLT    | "HR TOOHTER"       | HOT PEATE | HOT PLATE | SCRIB.I.D | 0        |
| CELL NAME                     | 312       | 571          | 512                | 761       | 762       | 783       | 784      |
|                               |           |              |                    |           |           |           | 4.000    |
| AREA (CM2)                    | 4.000     | 4.000        | 4.000              | 4.000     | 4.000     | 4.000     | . 062    |
| B.D. PHOCOHN-CM>              | 2.135     | 2.017        | 2.017              | 1.605     | 1.805     | 1.805     | 1.605    |
| A.D.R-SOR(OHM)                | .000      | 39.202       | 40.335             | 36.256    | 37.616    | 32.177    | 35.803   |
| AMO VOS (MV)                  | .000      | .000         | 575.000            | 570.000   | 574.000   | 132.000   | 116.000  |
| AMO ISC (MA)                  | .000      | .000         | 132.000<br>472.000 | 123.000   | 473.000   | 477.000   | 449.000  |
| AND INP (MY)                  | .000      |              | 124.000            | 114.000   | 121.000   | 126:000   | 109:000  |
| AND FILL FOTR                 | .000      | .000         | .771               | .756      | .779      | .762      | .760     |
| AND EFFICIENCY                | .000      | .000         | .108               | .098      | 573.000   | 561.000   | 550.000  |
| HHT VOC (HY)                  | .000      | .000         | 115.000            | 107.000   | 112.000   | 115.000   | 101.00   |
| AMI ISC (MH)                  | .000      | .000         | 477.000            | 465.000   | 474.000   | 482.000   | 450.000  |
| Ant IMP (MA)                  | .000      | .000         | 108.000            | 99.000    | 106.000   | 108.000   | 95.000   |
| AMI FILL FOTR                 | .600      | .600         | .779               | .736      | .763      | .779      | .10      |
| AMI EFFICIENCY                |           | 000          | 1.191 -            |           | 1.188     | 1.172     | 17163    |
|                               |           |              |                    |           |           |           |          |
| WHEN BROKEN                   | HOT PLATE | BACK ETCH    | 0                  | 0         | -6        | 0         | -0       |
| CELL_NAME                     | X2        | ×3           | ×4                 | ×5        | Né        | ×7        | ×e       |
|                               |           | 4.000        | 4.000              | 4.000     | 4.000     | 4.000     | 4.00     |
| THICK (CM)                    | 4.000     | 026          | .628               | .026      | .028      | .000      | .02      |
| B.D. PHOLOHM-CM)              | .000      | .000         | .000               | 40.335    | 42.146    | 39.862    | 41.24    |
| H.D.R-SORCOHM?                | 42,146    | 44.667       | 561 000            | 563.000   | 563.000   | 577.000   | - 581.00 |
| TAMO VOC (MV)                 | 139.000   | 139.000      | 140.000            | 133.000   | 138.000   | 130.000   | 135.00   |
| AMO 13C (MA)<br>AMO VMF (MV)  | 490.000   | 485.000      | 474.000            | 484.000   | 479.000   | 456.000   | 127.00   |
| AMO IMP (MH)                  | 132.000   | 129.000      | 130.000            | 126.000   | 130.000   | .693      | .76      |
| HMO FILL FOTR                 | .785      | .772         | .758               | .766      | .115      | .096      | .11      |
| AMO EFFICIENCY                | .117      | 584.000      | 582.000            | 564.000   | 503.000   | .000      | 581.00   |
| AMI VOC (MV)                  | 122.000   | 121.000      | 123.000            | 117.000   | 121.000   | .000      | 118.00   |
| AMI ISC (MA)                  | 497.000   | 482.000      | 483.000            | 485.000   | 484.000   |           | 155.00   |
| HMI IMP (MA)                  | 115.000   | 115.000      | 113.000            | 110.000   | 789       | .000      | .77      |
| AMI FILL FOTE                 | .766      | .784         | .762               | .781      | .139      | .000      | .13      |
| AMI EFFICIENCY                | 1140      | (139<br>(199 | 1:198-             | 1.184     | 1.209     |           | 1:19     |
|                               |           |              |                    |           |           |           |          |

## Table 18 continued

| CELL NAME         | 961     | 982   | 9#1     | 9M2     | 971    | 972     | ж1      |
|-------------------|---------|-------|---------|---------|--------|---------|---------|
|                   |         |       |         |         |        | 4.000   | 4.000   |
| AREA (CM2)        | 4.000   | 4.000 | 4.000   | 4.000   | 4.000  | .061    | .025    |
| THICK (CH)        | .061    | .061  | .062    | .062    | . 061  | 2.044   | .000    |
| B.D.RHO(OHM-CM)   | 1.658   | 1.658 | 1.523   | 1.523   | 2.044  | 38.522  | 57.330  |
| A.D.R-SOR(OHM)    | 43.054  | .000  | 39.882  | 39.202  | 39.662 |         | 580.000 |
| AMO VOC (MV)      | 559.000 | .000  | 581.000 | 562.000 | .000   | 561.000 | 143.000 |
| AMO ISC (MA)      | 116.000 | .000  | 130.000 | 131.000 | .000   | 130.600 | 475.000 |
| AMO VMP (MV)      | 454.000 | .000  | 461.000 | 481.000 | .000   | 482.000 |         |
| AMO IMP (MA)      | 110.000 | .000  | 123.000 | 124.000 | .000   | 124.000 | 134.000 |
| AMO FILL FCTR     | .770    | .000  | .783    | .762    | .000   | .791    | .767    |
| AND EFFICIENCY    | . 092   | .000  | .109    | .110    | .000   | .110    | 116     |
| ANT VOC THY       | 559.000 | .000  | 581.000 | 581.000 | .000   | 591.000 | 583.00  |
| ANT 15C (MA)      | 102.000 | .000  | 114.000 | 115.000 | .000   | 114.000 | 126.00  |
| AMI VHP (MV)      | 453.000 | .000  | 462.000 | 490.000 | .000   | 491.000 | 475.000 |
| ANT INP (MA)      | 96.000  | .000  | 108.000 | 107.000 | .060   | 109.000 | 118.000 |
| AMI FILL FOTE     | .763    | .000  | .766    | .765    | .000   | .792    | .76     |
| AMI EFFICIENCY    | .109    | .000  | .130    | .131    | .000   | .131    | .14     |
| "AMI EFF/HID EFF" | 1,178   | :000  | 1.190   | 7.189   | .000   | 1.167   | 1.19    |

Table 19

|                |      | SPECTRAL SE | ENSITIVITY- |       |      |      |      |
|----------------|------|-------------|-------------|-------|------|------|------|
|                |      | MH!         | 106-2       |       |      |      |      |
| CELL NAME      | 161  | 162         | 111         | 172   | 271  | 212  | 371  |
| w.t. emicPon . |      |             |             |       |      |      |      |
|                | .128 |             |             | .000  | .000 |      | .145 |
| .45            | .308 | .000        | .000        | .000  | .000 | .000 | .321 |
| .56            | .437 | .000        | .000        | . 600 | .000 | .000 | .439 |
| .55            | .475 | .000        | .000        | .000  | .000 | .000 | 7497 |
| .60            | .522 | .000        | .000        | .000  | .000 | .000 | .516 |
| .65            | .540 | .000        | .000        | .000  | .000 | .000 | .540 |
| .70            | .562 | .000        | .000        | .000  | .000 | .000 | .568 |
| .75            | .602 | .000        | .000        | .000  | .000 | .000 | .623 |
| .60            | .621 | .000        | .000        | .000  | .000 | .600 | .636 |
| . 65           | .612 | 000         | .000        | .000  | .000 | 000  | .660 |
| .90            | .612 | .000        | .006        | .000  | .000 | .600 | .705 |
| .95            | .271 | .000        | .000        | .000  | .000 | .000 | .607 |
| 1.05           | .176 | 400         |             | .000  | .000 | .000 | .227 |

Table 19 continued

|               |      | HAT        | 1CB-2  |      |      |      |      |
|---------------|------|------------|--------|------|------|------|------|
|               |      |            |        |      |      |      |      |
| CELL NAME     | 961  | 902        | 9H1    | 9m2  | 911  | 912  | ×1   |
| W.L. (MICRON) |      |            |        |      |      |      |      |
| .41           | :128 | .000       | .127   | .126 | .000 | .122 | .14  |
| .45           | .310 | .000       | .304   | .303 | .000 | .292 | .31  |
|               | .434 | .000       | 422    | 427  | .000 | .421 |      |
| .60           | .478 | .000       | .501   | .505 | .000 | .485 | .48  |
| .65           | .515 | .000       | .522   | .523 | .000 | .533 | .50  |
| .70           | .522 | .000       | .539   | .538 | .000 | .554 | .53  |
| .75           | .536 | .000       | .570   | .567 | .000 | .598 | .57  |
|               | .567 | 000        | -:602  | .590 | .000 | .629 | 62   |
| .90           | .485 | .000       | .590   | .565 | .000 | .632 | .66  |
| .95           | .305 | .000       | .473   | .467 | .000 | .551 | .62  |
| 1.05          | .086 | .000       | .153   | .149 | .000 | .197 | . 25 |
|               |      |            |        |      |      |      |      |
| CELL NAME     | 312  | 511        | 512    | 781  | 762  | 763  | 78   |
| W.L. (MICRON) |      |            |        |      |      |      |      |
| .41           | .000 | .000       | :125   | .116 | .122 | .122 | .12  |
| .45           | .000 | .000       | .295   | .301 | .365 | .305 | .30  |
|               | .000 | .000       | .495 - | 1465 | .429 | .484 | .42  |
| .60           | .000 | .000       | .517   | .476 | .469 | .502 | .49  |
| .65           | .000 | .000       | .547   | .484 | .499 | .513 | .50  |
| .70           | .000 | .000       | :571   | .480 | -497 | .517 | .512 |
| .75           | .000 | .000       | .621   | .485 | .50€ | .529 | .52  |
| . 80          | 000  | .000       | . 641  | .475 | .467 | .535 | .517 |
| .90           | .000 | .000       | .646   | .366 | .395 | .444 | .427 |
| .95           | .000 | .000       | .547   | .251 | .296 | .338 | .30  |
| 1.05          | .000 | .000       | .166   | .061 | .076 |      | .765 |
|               |      |            |        |      |      |      |      |
| CELL NAME     | ×2   | <b>X</b> 3 | ×4     | X5   | X6   | ¥7   | ×8   |
| W.L. (MICRON) |      |            |        |      |      |      |      |
| .41           | .121 | .139       | 136    | .137 | .143 | .118 | .733 |
|               | .280 | .309       | .304   | .292 | .326 | .293 | .308 |
|               |      | 424        | .420   | .365 | .449 | .419 | 425  |
| .55           | .450 | .500       | .472   | .453 | .459 | .470 | .502 |
| .65           | .504 | .521       | .522   | .478 | .504 | .454 | .53  |
| .70           | .530 | .549       | .550   | .510 | .526 |      | .55  |
| .75           | .570 | .591       | .590   | .554 | .576 | .520 | .54  |
| .80           | .605 | .632       | .626   | .605 | .621 | .574 | .569 |
| .90           | .664 | .679       | .646   | .691 | .710 | .585 | .593 |
| .95           | .624 | .644       | .629   | .642 | .662 | .604 | .634 |
| 1.05          | .256 | .269       |        | .268 | 275  | .204 | 7215 |

Table 20 DARK CURRENT DENSITY, BUN Hame8-2

| V <sub>p</sub> /S/S | C1     | C2     | c)     | C4     | C5     | C6     | C7     | CB     |
|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| .01 Volta           | 1.5-07 | 2.3-08 | 6.6-06 | 1.6-07 | 1.7-96 | 1.8-26 | 3.8-06 | 1.7-06 |
| .04                 | 5.7    | 1.4-07 | 2.6-05 | 6.8    | 4.4    | 7.4    | 1.9-05 | 6.8    |
| .08                 | 1.2-06 | 5.3    | 5.3    | 1.9-06 | 1.1    | 1.4-05 | 3.1    | 1.4-95 |
| .10                 | 1.5    | 9.4    | 6.7    | 2.9    | 1.1-05 | 1.6    | 4.0    | 1.0    |
| .15                 | 2.7    | 3.1-06 | 1.1-04 | 9.1    | 1.7    | 2.7    | 6.2    | 3.1    |
| .20                 | 4.8    | 8.3    | 1.5    | 2.6-05 | 2.5    | 1.6    | 9.0    | 5.0    |
| . 25                | 9.2    | 1.8-05 | 1.9    | 6.5    | 3.6    | 4.7    | 1.3-04 | 7.9    |
| . 30                | 2.0-05 | 3.5    | 2.4    | 1.7-04 | 5.2    | 6.1    | 1.9    | 1.2-0  |
| . 35                | 4.7    | 6.2    | 2.8    | 2.6    | 7.9    | 8.5    | 3.0    | 1.9    |
| .40                 | 1.2-04 | 1.2-04 | 3.1    | 4.6    | 1.4-04 | 1.4-04 | 5.1    | 2.7    |
| .45                 | 3.6    | 2.6    | 3.9    | 1.4    | 3.0    | 1.0    | 9.7    | 4.1    |
| .52                 | 1.2-03 | 9.7    | 4.6    | .8-03  | 1.0-03 | 1.0-03 | 2.2-03 | 6.5    |
| v <sub>a</sub>      |        |        |        |        |        |        |        |        |
| .05 Vo.13           | 1.0-06 | 6.3-08 | 3.3-05 | 1.2-07 | 5.4-06 | 9.5-06 | 1.9-05 | 8.5-0  |
| .10                 | 2.2    | 6.8    | 6.6    | 1.5-66 | 1.1-05 | 1.9-05 | 3.8    | 1.7-0  |
| .20                 | 5.0    | 1.2-07 | 1.3-04 | 3 4    | 2.1    | 4.0    | 7.5    | 3.4    |
| . 30                | 8.1    | 1.4    | 2.0    | 5.6    | 3.2    | 6.3    | 1.1-04 | 5.1    |
| .40                 | 1.2-05 | 1.5    | 2.6    | 11.1   | 4.3    | 8.7    | 1.5    | 6.8    |
| .50                 | 1.5    | 1.7    | 3.4    | .1-05  | 5.4    | 1.1-04 | 1.9    | 8.5    |
| .60                 | 2.0    | 1.9    | 4.2    | 1.3    | 6.4    | 1.4    | 2.3    | 1.0-0  |

| V <sub>y</sub> 178 | 371    | 572    | 912    | 9111   | 9%2    | 191    | 781    | 78.2   | 783    | 784    | 981    |
|--------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| .61 Vo.14          | 1.6-06 | 1.3-18 | 1.5-09 | 5.8-08 | 3.5-08 | 6.8-08 | 7.5-09 | 5.0-09 | 2.5-08 | 3.5-08 | 3.0-07 |
| .04                | 1.0-05 | 5.3    | 4.3-06 | 2.7-07 | 2.0-07 | 3.1-07 | 4.5-08 | 2.8-08 | 1.1-07 | 1.9-07 | 1.0-06 |
| .00                | 2.9    | 1.6-07 | 1.3-07 | 4.9    | 6.6    | 7.7    | 1.3-07 | 8.0    | 2.9    | 6.1    | 3.9    |
| .10                | 4.2    | 2.5    | 2.0    | 6.4    | 1.0-06 | 1.1-06 | 2.1    | 1.2-07 | 4.4    | 1.0-06 | 5.7    |
| .15                | 9.3    | 7.3    | 5.4    | 1.1-06 | 2.6    | 2.7    | 6.0    | 3.2    | 1.1-06 | 3.3    | 1.3-05 |
| .20                | 1.4-14 | 2.1-06 | 1.4-06 | 2.0    | 5.8    | 6.0    | 1.8-06 | 8.9    | 3.0    | 9.1    | 2.3    |
| .25                | 2.0    | 5.7    | 1.2    | 3.8    | 1.2-05 | 1.2-05 | 5.3    | 2.5-06 | 7.1    | 2.2-05 | 3.9    |
| .30                | 2.7    | 1.5+05 | 7.7    | 8.6    | 2.4    | 2.7    | 1.6-05 | 8.4    | 1.8-05 | 4.6    | 6.5    |
| . 75               | 3.6-04 | 3.8    | 2.0-05 | 2.2-05 | 5.1    | 6.0    | 5.2    | 3.1-05 | 4.7    | 1.1-04 | 1.2-04 |
| .40                | 4.9    | 1.0-04 | 5.9    | 6.6    | 1.2-04 | 1.4-04 | 1.8-04 | 1.2-04 | 1.4-04 | 3.0    | 2.4    |
| .45                | 7.3    | 3.4    | 2.2-04 | 2.4-04 | 3.4    | 4.2    | 6.7    | 5.2    | 4.5    | 1.0-03 | 6.7    |
| .50                | 1.6-03 | 1.3-03 | 1.0-03 | 9.6    | 1.3-03 | 1.5-03 | 2.5-03 | 2.1-03 | 1.6-03 | 3.9    | 2.2-03 |
| v <sub>R</sub>     |        |        |        |        |        |        |        |        |        |        |        |
| .05 Valls          | 5.2-06 | 2.5-08 | 2.8-08 | 2.8-07 | 9.0-08 | 1.6-07 | 3.5-08 | 2.5-08 | 6.5-08 | 1.5-07 | 1.3-06 |
| .10                | 7.4    | 4.5    | 4.3    | 5.5    | 1.3-07 | 2.9    | 6.8    | 5.0    | 1.1-07 | 2.8    | 2.5    |
| .20                | 1.0-05 | 7.0    | 7.0    | 1.1-06 | 1.8    | 5.8    | 1.3-07 | 1.1-07 | 1.0    | 5.9    | 5.8    |
| . 10               | 1.4    | 9.5    | 9.5    | 1.7    | 2.2    | 9.2    | 2.2    | 2.0    | 2.4    | 9.9    | 1.0-05 |
| .40                | 1.7    | 1.2-07 | 1.2-07 | 2.4    | 2.5    | 1.3-06 | 3.3    | 3.0    | 3.0    | 1.5-06 | 1.6    |
| .50                | 2.0    | 1.5    | 1.4    | 3.0    | 2.6    | 1.8    | 4.7    | 4.4    | 3.5    | 2.2    | 2.3    |
| .60                | 2.4    | 1.7    | 1.7    | 3.7    | 3.2    | 2.3    | 6.6    | 6.0    | 4.1    | 3.0    | 3.1    |
|                    |        |        |        |        |        |        |        |        |        |        |        |

Table 21
PESISTIVITY AND ILLUMINATED CHARACTERISTICS

HAMCO-1

| CELL NAME                         | 181     | 162                | 171           | 172          | 173     | 381     | 362      |
|-----------------------------------|---------|--------------------|---------------|--------------|---------|---------|----------|
|                                   | 4.000   | 4.000              | 4.000         | 4.000        | 4.000   | 4.000   | 4.000    |
| THICK COMS                        | .060    | .060               | .061          | .001         | .061    | .061    | 061      |
| B.D.RHO(OHM-CM)                   | .189    | .169               | .332          | .332         | .332    | .221    | .221     |
| H.D.P-SOR OHM)                    | 53.476  | 53.931             | 49.652        | 53.470       | 51.665  | 55.290  | 57.103   |
| And VOC (MV)                      | 467.000 | .000               | 546.000       | 595.000      | 571.000 | 417.000 | 000      |
| AND ISC (MA)                      | 117.000 | .000               | 150.000       | 147.000      | 138.000 | 250.000 | .000     |
| AND VIP (MV)                      | 325.000 | .000               | 491.000       | 125.000      | 123.000 | 87.000  |          |
| HIO THE (MH)                      | .508    | .000               | 152.000       | .699         | 773     | .450    | .000     |
| AMO FILL FOTR                     | .053    | .000               | .120          | .113         | .107    | .040    | .000     |
| ANT VOC CHV                       | .000    | .000               | .000          | .000         | 570.000 | .000    | .000     |
| AMI ISC (MA)                      | .000    | .000               | .000          | .000         | 119.000 | .000    | .000     |
| AMI VMP (MV)                      | .000    | .000               | .000          | .000         | 468.000 | .000    | .000     |
| ent Inp (Me)                      | .000    | .000               | .000          | .000         | 106.000 | .000    | .000     |
| AMI FILL FOTR                     | .000    | .000               | .000          | .000         | .731    | .000    | .000     |
| AMI EFFICIENCY                    | .000    | .000               | .000          | .000         | 1.164   | .000    | .000     |
| AMI EFFZAND EFF                   | .000    | .000               | . 000         | .040         | 1.104   | .000    | .000     |
| WHEN BROKEN                       |         | 0                  | 0             | - 0          | 0       | -0      | 0        |
| CELL NAME                         | 371     | 372                | 561           | 562          | 511     | 512     | 761      |
|                                   |         |                    |               |              | 4.000   | 4.000   | 4.000    |
| AREA (CH2)                        | 4.000   |                    | 4.000<br>.061 | 4.000        |         | .061    | .061     |
| THICK (CM)                        | .070    | .222               | .249          | .249         | .249    | .249    | .221     |
| B.D.RHO(OHM-CM)<br>A.D.R-SOR(OHM) | 53.024  | 53.431             | 54.364        | 56.650       | 56.650  | 54.384  | 57.103   |
| AHO VOC (MV)                      | 000     | 601.000            | 560.000       | 577.000      | 557.000 | 521.000 | 575.000  |
| And ISC (Mm)                      | .000    |                    | 131.000       | 134.000      | 144.000 | 146.000 | 136.000  |
| AND YMP (MY)                      | .000    | 495.000            | 462.000       | 475.000      | 385.000 | 338.000 | 470.000  |
| AMO IMP (NH)                      | .000    | 131.000            | 120.000       | 123.000      | 106.000 | 112.000 | 724.000  |
| AMO FILL FETR                     | .000    | .734               | .756          | .756         | .509    | .498    | .109     |
| AMO EFFICIENCY                    | .000    | .120               | 557.000       | - 576 .000 - |         | :000    | 573.000  |
| ANT VOC CHYD                      | .000    | 127.000            | 112.000       | 116.600      | .000    | .000    | 117.000  |
| Ami 150 (ma)                      | .000    | 493.000            | 459.000       | 475.000      | .000    | .000    | 472.000  |
| AMI VMP (MV)                      | .000    | 116.000            | 104.000       | 105.000      | .000    | .000    | 108.000  |
| ANI FILL FOTE                     | .000    | .769               | .765          | .746         | .000    | .000    | .760     |
| AMI EFFICIENCY                    | .000    | .145               | .119          | .125         | .000    | .000    | .127     |
| AMI EFFZAMO EFF                   | :000-   | 1.214              | 1.165         | 1:155        | .600    | :-:000  | T.183    |
| WHEN BROKEN                       | -,      |                    |               | - 0          | -c-     |         | PRINTING |
|                                   |         |                    |               |              |         |         |          |
| CELL NAME                         | 711     | 712                | 9m1           | 9/12         | 9113    |         | 912      |
| ekse (Ch2)                        | 4.000   | 4.000              | 4.000         | 4.000        | 4.000   | 4.000   | 4.000    |
| THICK COME                        | .061    | .061               | .060          | .060         | . 000   | 130.    | .061     |
| B.D.RHO OHM-CM>                   | .221    | .221               | .216          | .216         | .216    | .221    | 53.024   |
| A.D.P-SORCOHMO                    | 56.650  | 54.364             | 53.024        | 54.384       | 54.364  | 57.556  | 602.000  |
| AMO VOC KMV>                      | 601.000 | 594.000            | 597.000       | 142.000      | 138.000 | 144.000 | 147.000  |
| AMO ISC (MA)                      | 504.000 | 143.000<br>488.000 | 500.000       | 500.000      | 250.000 | 300.000 | 505.000  |
| AND INF (NA)                      | 135.000 | 115.000            | 129.000       | 124.000      | 99.000  | 73.000  | 135.000  |
| AMO FILL FOTP                     | .770    | .661               | .772          | .734         | .444    | .265    | .770     |
| AND EFFICIENCY                    | .126    | .104               | .119          | .115         | . 046   | .040    | .126     |
| HHI VOC (MV)                      | 660.000 | .000               | 595.000       | 593.000      | .000    | 000     | 599.000  |
| AM1 ISC (MH)                      | 127.000 | .000               | 122.000       | 122.000      | .000    | .000    | 496.000  |
| AMI VMP (MV)                      | 504.000 | .000               | 497.000       | 491.000      | .000    | .000    | 117.000  |
| AMI IMP (MA)                      | 118.000 | .000               | .760          | .733         | .000    | .000    | .763     |
| AMI FILL FOTR                     | .750    | .000               | .136          | .133         | .000    | .000    | .145     |
| AMI EFFZAMO EFF                   | 1.163   |                    | 1.157         | 1.157        |         |         | T.152    |

Table 21 continued

|  |  | HAM         | co-1   |   |  |  |  |
|--|--|-------------|--|---|--|--|--|
|  | .,   |             |  |   |  |  |  |
| CELL HAME  | ×1   | . x2        | хз   | X4  | xs   | ×6   | X7   |
| HEEH (CM2)   | 4.000  | 4.000       | 4.000  | 4.000   | 4.000  | 4.000  | 4.00   |
| THICK (CH)   | . 023  | .023        | .021   | .0.3  | .023   | .000   | .02  |
| B.D. RHOL OHM-CH)  | 57.024   | 50.758      | 51.665   | 52.116  | 54.384   | 53.931   | 52.57  |
| A.D.R-SOR(OHM)   | 560.000  |             | 561.000  |   | 572.600  |  | - 577.00   |
| AND ISC (MA)   | 142.000  | .000        | 142.000  | .000  | 142.000  | .000   | 142.60   |
| AND VMP (HV)   | 131.000  |             | 131.000  | .000  | 125.000  | .600   | 130.00   |
| AND THE (MA)   | .763   | .000        | .772   | .000  | .754   | .000   | .75  |
| AND EFFICIENCY   | .116   | .000        | .116   | .000  | 113  | .000   |  |
| ANT VOC (MV)   | 575.000  | .000        | 123.000  | .000  | 124.000  | .000   | 124.60   |
| AMI ISC (MA)   | 473.000  | .000        | 461.000  | .000  | 472.000  | .000   | 470.00   |
| AMI IMP (MA)   | 115.000  | .000        | 114.000  | .000  | 116.000  |  | 116.00   |
| AMI FILL FOTE  | .769   | .000        | .767   | .000  | .765   | .000   | .76  |
| AMI EFFICIENCY   | 17176  | :000        | 1.165  |   | - T.209  | : 660  | T.18   |
|  |  |             |  |   |  |  |  |
| WHEN BROKEN  |  | FAINTING -  |  | 3   | •  | 7  |  |
| CELL HAME  | ко   |             |  |   |  |  |  |
|  |  |             |  |   |  |  |  |
| AFEA (CH2)   | 4.000  |             |  |   |  |  |  |
| THILF LEND   | . 623  |             |  |   |  |  |  |
| B.O. PHOCOHN-CH)   | 51.665   |             |  |   |  |  |  |
| AND VOC THUS   | .000   |             |  |   |  |  |  |
| AMO ISC (MA)   | .000   |             |  |   |  |  |  |
| AHO VHP (HV)   | .000   |             |  |   |  |  |  |
| AND FILL FCTP  | .000   |             |  |   |  |  |  |
| AND EFFICIENCY   | .000   |             |  |   |  |  |  |
| 7H1 VOC (HV)   | .000   |             |  |   |  |  |  |
| ANI ISC (MA)   | .000   |             |  |   |  |  |  |
| the same of the sa | .000 -   |             |  |   |  |  |  |
| AMI THE (MA)   |  |             |  |   |  |  |  |
| AHI FILL FCTP  | .000   |             |  |   |  |  |  |
|  |  |             |  |   |  |  |  |
| ANT EFFICIENCY   | .000   | Table       | 22   |   |  |  |  |
| AMI FILL FCTP  | .000   | Table       |  |   |  |  |  |
| ANT EFFICIENCY   | .000   | SECTION SE  | meltivity.   |   | •  |  |  |
| ANT EFFICIENCY   | .000   | SECTION SE  |  |   |  |  |  |
| ANT EFFICIENCY   | .000   | SECTION SE  | meltivity.   |   | 1113   | 361  | 362  |
| AMI FILL FCTP AMI EFFICIENCY TANT EFFZAMO EFF  OTHER ENGIETE  CELL NAME  | .000   | SHEETKHL SE | 000-1  |   | . 173  | 361  | 362  |
| CELL NAME  | . 000<br>. 200<br>. 000  |             |  |   |  |  |  |
| CELL NAME  U.L. (MICFON)   | .123   | 162         | 111  | 114.  | .117   | .103   | .136   |
| CELL NAME  W.L. (MICFON)  ANI FILL FCTP  ANI EFFZAND EFF  COUNTY  CELL NAME  W.L. (MICFON)  .41 .45  | .000<br>.200<br>.000   |             |  | 114   | .117   | .103<br>.254<br>.365                                 | .136   |
| CELL HAME  U.L. (MICPON)  41  45  50  50   | 161<br>-123<br>-265<br>-372<br>-428                                |             |  | 112   | .117<br>.257<br>.762<br>.436                         | .103<br>.254<br>.365                                 | .136   |
| CELL NAME  W.L. (MICFON)  ANI FILL FCTP  ANI EFFZAND EFF  COUNTY  CELL NAME  W.L. (MICFON)  .41 .45  | .000<br>.200<br>.000   |             | 111<br>111<br>111<br>111<br>111<br>111<br>111<br>111 |   | .117   | .103<br>.254<br>.365<br>.402<br>.417                 | .136<br>.254<br>.371<br>.417                                 |
| CELL HAME  U.L. (MICFON)  41  45  50  65  76   | 161<br>- 123<br>- 268<br>- 372<br>- 428<br>- 451<br>- 465          |             | 111<br>  |   | 117<br>257<br>792<br>478<br>472<br>472<br>525        | 103<br>.254<br>.3.5<br>.402<br>.417<br>.415          | .136<br>.254<br>.371<br>.417<br>.426<br>.425                 |
| CELL HAME  U.L. (MICFON)  A1  A5  A6  A6  A7  A7  A7  A7  A7  A7  A7  A7   | 161<br>-123<br>-265<br>-372<br>-428<br>-451<br>-465<br>-499        |             |  | 171<br>172<br>173<br>169<br>169<br>175<br>175<br>175<br>175<br>175<br>175<br>175<br>175<br>175<br>175 | 117<br>257<br>782<br>472<br>472<br>494<br>555        | .103<br>.254<br>.365<br>.402<br>.417<br>.418         | .136<br>.254<br>.371<br>.417<br>.426<br>.425                 |
| CELL NAME  U.L. (MICPON)  .41 .55 .60 .75 .60  | .000<br>.000<br>.000   |             | 111<br>  |   | 117<br>257<br>792<br>478<br>472<br>472<br>525        | 103<br>.254<br>.3.5<br>.402<br>.417<br>.415          | .136<br>.254<br>.371<br>.417<br>.426<br>.425<br>.443<br>.431 |
| CELL NAME  L. (MICFON)  CELL NAME  L. (MICFON)  | 161<br>- 123<br>- 265<br>- 372<br>- 451<br>- 465<br>- 494<br>- 495 |             |  |   | 117<br>257<br>762<br>479<br>472<br>494<br>525<br>559 | .103<br>.254<br>.365<br>.402<br>.417<br>.416<br>.407 | .136<br>.254<br>.371<br>.417<br>.426<br>.425                 |

Table 22 continued

|               |       | на   | 100-1 |       |      |      |      |
|---------------|-------|------|-------|-------|------|------|------|
|               |       |      |       |       |      |      |      |
| CELL III E    | 371   | 312  | 561   | 502   | 5T1  | 572  | 76   |
| W.L. (MICROIL |       |      |       |       |      |      |      |
|               | 141   | .145 | .113  | .110  | .125 | .125 | .111 |
| .45           | .247  | .245 | .261  | .251  | .270 | .266 | .26  |
| .55           | .453  | .457 | .422  | .416  | .448 | .452 | .40  |
| .60           | .501  | .494 | .448  | .448  | .491 | .495 | .45  |
| .70           | .523  | .524 |       | .466  | .513 | .567 |      |
| .75           | .617  | .637 | .435  | .519  | .606 | .612 | .49  |
| .65           | 670   | 716  | 4.70  | 523   | :671 | .657 | .50  |
| .90           | .743  | .617 | .427  | .493  | .739 | .740 | .42  |
| .95           | ,786  | .650 | .300  | 1115  | .749 | .751 | .29  |
| 1.05          | . 391 | .367 | . 543 | .115  | .350 | .346 | . 07 |
|               | * *   |      |       |       |      |      |      |
| CELL NAME     | 711   | 712  | 9M1   | 9112  | 9#3  | 971  | 91.  |
| W.L. (MICRON) |       |      |       |       |      |      |      |
| .41           | .125  | 172  |       | .116  | .128 | .121 | .16  |
| .45           | .257  | .270 | .243  | .259  | .271 | .264 | .30  |
| .50           | .390  | .300 | 374   | .396  | .370 | .390 | .39  |
| .55           | .465  | .439 | 477   | .436  | .462 | .452 | .45  |
| .65           | .521  | .500 | .496  | .501  | .485 | .523 | .51  |
| .70           | .540  | .563 | .521  | .532  | .519 | .565 | .57  |
| .75           | .127  | .605 | .550  | .565  | .544 | .666 | .61  |
| .65           | .670  | .666 | .576  |       | .556 | .668 | 66   |
| .90           | .784  | .829 | .539  | .562  | .561 | .704 | .74  |
| 1.05          | 263   | 305  | :163  |       | :179 | 337  | 35   |
|               |       |      |       |       |      |      |      |
| CELL NAME     |       | X2   |       | X4    | ×5   | X6   | ×7   |
| W.L. (MICRON) |       |      |       |       |      |      |      |
| .41           | .104  | .000 | .111  | .137  | .114 | .257 | .10  |
| .45           | .249  | .000 | .260  | .281  | .268 | .385 | .25  |
| .55           | .448  | .000 | .440  | 7.463 | .450 | .467 | .45  |
| .60           | .466  | .000 | .519  | .507  | .490 | .498 | .50  |
| 7.0           | .519  | .000 | 555   | .531  | 550  | .633 | .57  |
| .75           | .606  | .000 | .062  | .630  | .592 | .648 | .61  |
| .85           | .662  | :000 | .651  |       |      |      | 65   |
| .90           | .705  | .000 | .668  | .776  | .648 | .916 | .66  |
| .95           | .666  | .000 | .642  | .612  | .606 | .824 | .64  |
| 1.05          | .277  | .000 | .255  | .410  | .276 | .472 |      |
| CELL NAME     | ×9.   |      |       |       |      |      |      |
| W.L. (MICRON) |       |      |       |       |      |      |      |
| .41           | .165  |      |       |       |      |      |      |
| .50           | .397  |      |       |       |      |      |      |
| .55           | .457  |      |       |       |      |      |      |
| .60           | .461  |      |       |       |      |      |      |
| .70           | .626  |      |       |       |      |      |      |
| .75           | .653  |      |       |       |      |      |      |
|               | 655   |      |       |       |      |      |      |
| .90           | .622  |      |       |       |      |      |      |
| .95           | .750  |      |       |       |      |      |      |

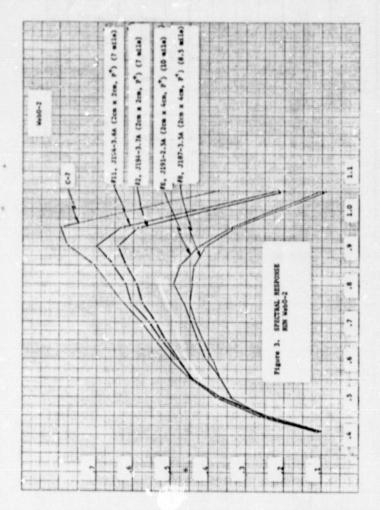
Table 23 DANK CURRENT DENSITY, BUN Has 8-1

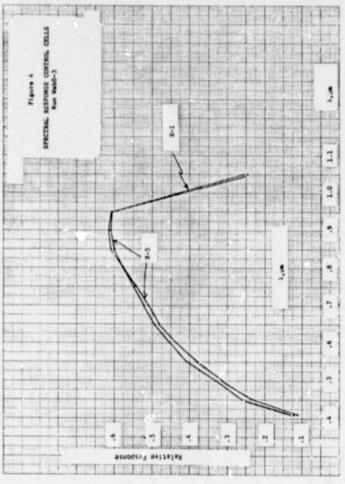
| Vp/E.'N        | C1     | 63     | C.     | C5     | 76     | c)     | V <sub>p</sub> /S/N | 721    | 712    | 771    | 9M1    | 942    | 983    |
|----------------|--------|--------|--------|--------|--------|--------|---------------------|--------|--------|--------|--------|--------|--------|
| .0: 791ts      | 2.6-07 | 4.4-06 | 5.9-05 | 4.6-06 | 5.2-04 | 1.6-06 | .01 Volts           | 7.7-06 | 8.9-05 | 6.4-06 | 1.1-05 | 6.2-05 | 1.1-04 |
| .04            | 1.4-06 | 1.9-05 | 2.4-04 | 1.9-05 | 1.8-03 | 5.4    | .04                 | 2.6-05 | 3.1-04 | 2.3-05 | 4.0    | 1.8-04 | 4.7    |
| .08            | 4.4    | 4.7    | 4.5    | 4.7    | 4.2    | 1.2-05 | 01                  | 4.8    | 5.0    | 4.3    | 7.5    | 3.5    | 1.6    |
| .10            | 7.1    | 7.4    | 5.8    | 7.4    | 5.7    | 1.6    | .10                 | 6.1    | 7.2    | 5.6    | 9.3    | 4.3    | 1.3-03 |
| -11            | 1.9-05 | 1.4-94 | 1.0-03 | 1.4-04 | 1.0-02 | 3.3    | .15                 | 2.6-04 | 1.1-03 | 1.2    | 1.4-04 | 6.6    | 2.5    |
| .25            | 3.9    | 2.4    | 1.5    | 2.4    | 1.6    | 5.1    | .20                 | 3.5    | 1.5    | 1.1-04 | 1.9    |        | 4.7    |
| .25            | 7.4    | 3.6    | 2.0    | 3.6    | 2.3    | 8.0    | .25                 | 4.5    | 1.9    | 1.4    | 2.4    | 1.1-03 | 1.1    |
| . 30           | 1.2004 | 5.0    | 2.6    | 5.0    |        | 1.2-04 | .32                 | 5.7    | 2.4    | 1.8    | 3.0    | 1.4    | 1.3-02 |
| . 35           | 1.5    | 6.4    | 3.1    | 6.4    |        | 1.9    | .35                 | 6.0    | 2.9    | 2.2    | 3.7    | 1.6    | 1.7    |
| .40            | 3.1    | 6.4    | 3.7    | 1.4    |        | 3.1    | .40                 | 0.1    | 3.4    | 3.0    | 4.6    | 1.9    | 2.5    |
| .45            | 5.5    | 1.1-03 | 4.4    | 1.1-03 |        | 6.0    | .45                 | 9.9    | 4.2    | 7.1    | 7.0    | 2.4    |        |
| .50            | 1.4-03 | 2.0    | 5.0    | 2.0    |        | 1.7-03 | .50                 | 1.2-03 | 5.2    | 1.0-03 | 1.6-03 | 3.4    |        |
| v <sub>p</sub> |        |        |        |        |        |        | v <sub>k</sub>      |        |        |        |        |        |        |
| .05 Tolts      | 8.4-04 | 9.2-06 | 2.5-04 | 9.2-06 | 2.3-03 | 6.3-06 | .05 Volts           | 3.0-05 | 3.8-94 | 3.2-05 | 4.7-05 | 2.0-04 | 5.3-04 |
| .10            | 1.3-03 | 1.5-05 | 4.2    | 1.5-05 | 4.2    | 1.3-05 | .10                 |        | 8.0    | 6.2    | 9.5    | 4.4    | 1.0-03 |
| .20            | 2.1    | 2.0    | 8.1    | 2.0    | 8.2    | 2.4    | .20                 | 1.2-04 | 1.7-03 | 1.3-04 | 2.0-04 | 1.9    | 2.0    |
| .30            | 2.8    | 2.5    | 1.2-03 | 2.4    | 1.2-02 | 3.5    | . 30                | 1.9    | 2.7    | 2.1    | 3.0    | 1.3-03 | 3.1    |
| .43            | 3.6    | 3.1    | 1.6    | 2.9    | 1.6    | 4.5    | .40                 | 4.1    | 3.8    | 3.0    | 4.1    | 1.0    | 4.1    |
| .50            | 4.3    | 3.6    | 2.0    | 3.3    | 2.1    | 5.6    | .50                 | 7.3    | 5.1    | 3.7    | 5.1    | 2.3    | 5.2    |
| .60            | 5.0    | 4.2    | 2.4    | 3.8    | 2.5    | 6.7    | .60                 |        | 6.5    | 5.0    | 6.3    | 2.8    | 6.2    |

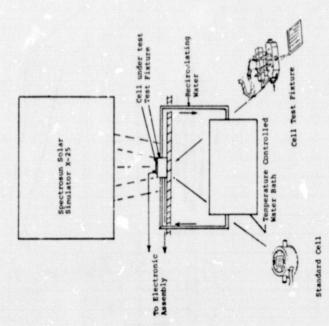
Table 23 continued

| .01 Volte  | V, 2, 8        | 251    | 35.2   | 59.    | 552    | 571    | 572    | 371    | 27.1   |
|--|----------------|--------|--------|--------|--------|--------|--------|--------|--------|
| .08  |                |        | 8.3-06 | 5.4-06 | 1.0+05 | 1.1-05 |        | 1.3-05 | 5.9-06 |
| .10  | .04            | 6.0-05 | 2,7+06 | 2.2-05 | 1.7    | 4.6    | 1.4-04 | 5.7    | 2.5-05 |
| .15 9.6 1.5-24 8.0 1.4-04 1.7 7.3 2.2 9.8  | .03            | 2.0-04 | 7.4    | 4.2    | 7.5    | 9.2    | 1.0    | 1.2-04 | 5.1    |
| .25  | .10            | 3.2    | 9.6    | 5.2    | 9.3    | 1.2-04 | 4.0    | 1.5    | 6.4    |
| .25  | .15            | 9.6    | 1.5-04 | 8.0    | 1.4-04 | 1.7    | 7.3    | 2.2    | 9.8    |
| .32  | .25            | 2.4-03 | 2.1    | 1.1-04 | 2.0    | 2.3    | 1.3-03 | 3.1    | 1.3-04 |
| .35  | .25            | 4.7    | 2.8    | 1.4    | 2.6    | 2.9    | 2.2    | 3.9    | 1.7    |
| .40  | . 32           | 8.0    | 3.4    | 1.8    | 3.2    | 3.4    | 3.7    | 4.8    | 2.2    |
| .45  | . 35           | 1.2-02 | 4.1    | 2.6    | 4.2    | 3.6    | 5.7    | 5.8    | 2.6    |
| V <sub>R</sub> .05 Volts     4.7-05     4.3-05     2.7-05     5.0-05     4.6-05     1.7-04     1.1-04     3.2-05       .10     8.7     8.6     5.6     1.0-04     9.4     3.5     2.0     6.4       .20     1.7-04     1.7-04     1.2-04     2.2     1.9-04     7.1     4.7     1.3-04       .30     2.7     2.6     1.8     3.5     2.9     1.1-03     7.7     1.9       .41     3.8     3.6     2.5     4.7     3.9     1.5     1.1-03     2.6       .50     4.9     4.6     3.3     6.2     4.8     1.9     1.6     3.3   | .40            | 1.8    | 4.9    | 4.5    | 6.0    | 3.9    | 1.4    | 7.5    | 3.1    |
| V <sub>R</sub> .05 Volts         4.7-05         4.3-05         2.7-05         5.0-05         4.6-05         1.7-04         1.1-04         3.2-05           .10         8.7         8.6         5.6         1.0-04         9.4         3.5         2.0         6.4           .20         1.7-04         1.7-04         1.2-04         2.2         1.9-04         7.1         4.7         1.3-04           .30         2.7         2.6         1.8         3.5         2.9         1.1-03         7.7         1.9           .41         3.8         3.6         2.5         4.7         3.9         1.5         1.1-03         2.6           .50         4.9         4.6         3.3         6.2         4.8         1.9         1.6         3.3 | .45            | 2.4    | 5.8    | 1.0-03 | 1.1-03 | 4.2    | 1.2-02 | 8.7    | 3.6    |
| .05 Volts 4.7-05 4.3-05 2.7-05 5.0-05 4.6-05 1.7-04 1.1-04 3.2-05 1.0 8.7 8.6 5.6 1.0-04 9.4 3.5 2.0 6.4 1.20 1.7-04 1.7-04 1.2-04 2.2 1.9-04 7.1 4.7 1.3-04 1.2 2.7 2.6 1.8 3.5 2.9 1.1-03 7.7 1.9 1.1 3.8 3.6 2.5 4.7 3.9 1.5 1.1-03 2.6 1.5 4.9 4.6 3.3 6.2 4.8 1.9 1.6 3.3   | .50            |        | 6.5    | 3.7    | 2.9    | 4.5    | 1.6    | 9.9    | 4.2    |
| .10 8.7 8.6 5.6 1.0-04 9.4 3.5 2.0 6.4 .20 1.7-04 1.7-04 1.2-04 2.2 1.9-04 7.1 4.7 1.3-04 .30 2.7 2.6 1.8 3.5 2.9 1.1-03 7.7 1.9 .41 3.8 3.6 2.5 4.7 3.9 1.5 1.1-03 2.6 .50 4.9 4.6 3.3 6.2 4.8 1.9 1.6 3.3  | v <sub>R</sub> |        |        |        |        |        |        |        |        |
| .20 1.7-04 1.7-04 1.2-04 2.2 1.9-04 7.1 4.7 1.3-04 .22 2.5 2.9 1.1-03 7.7 1.9 .25 2.5 4.7 3.9 1.5 1.1-03 2.6 .25 4.9 4.6 3.3 6.2 4.8 1.9 1.6 3.3   | .05 Volts      | 4.7-05 | 4.3-05 | 2.7-05 | 5.0-05 | 4.6-05 | 1.7-04 | 1.1-04 | 3.2-05 |
| .33 2.7 2.6 1.8 3.5 2.9 1.1-03 7.7 1.9<br>.41 3.8 3.6 2.5 4.7 3.9 1.5 1.1-03 2.6<br>.52 4.9 4.6 3.3 6.2 4.8 1.9 1.6 3.3  | .10            | 8.7    | 8.6    | 5.6    | 1.0-04 | 9.4    | 3.5    | 2.0    | 6.4    |
| .11 3.8 3.6 2.5 4.7 3.9 1.5 1.1-03 2.6<br>.50 4.9 4.6 3.3 6.2 4.8 1.9 1.6 3.3  | .20            | 1.7-04 | 1.7-04 | 1.2-04 | 2.2    | 1.9-04 | 7.1    | 4.7    | 1.3-04 |
| .50 4.9 4.6 3.3 6.2 4.8 1.9 1.6 3.3  | . 33           | 2.7    | 2.6    | 1.8    | 3.5    | 2.9    | 1.1-03 | 7.7    | 1.9    |
|  | .45            | 3.8    | 3.6    | 2.5    | 4.7    | 3.9    | 1.5    | 1.1-03 | 2.6    |
| .60 6.2 5.7 4.1 7.7 5.9 2.4 2.2 4.0  | .60            | 4.9    | 4.6    | 3.3    | 6.2    | 4.8    | 1.9    | 1.6    | 3.3    |
|  | .60            | 6.2    | 5.7    | 4.1    | 7.7    | 5.9    | 2.4    | 2.2    | 4.0    |

#### 8.0 FIGURES







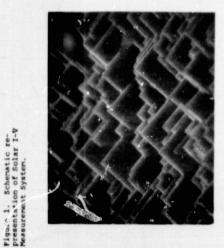


Figure 2

TEXTURED SURFACE OF SOLAR CELL
NAGH FOTHAM
SCANNING ELECTRON MICROSCOPE
SECONDARY ELECTRONS, ~50° TILT, 1500X

ORIGINAL PAGE IS OF POOR QUALITY

